

Introduction to the Stiffness (Displacement) Method

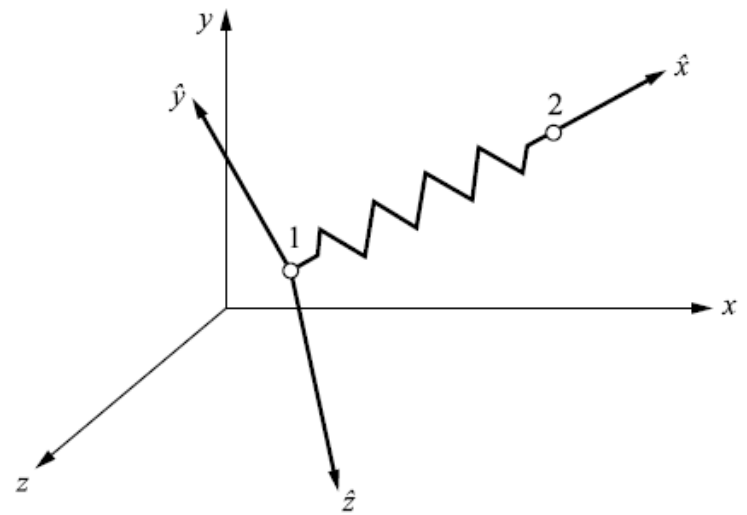
Definition of the Stiffness Matrix

$$\underline{\hat{f}} = \underline{\hat{k}} \underline{\hat{d}}$$

Element stiffness equation in
local coordinate system

$$\underline{F} = \underline{K} \underline{d}$$

Global stiffness equation in global
coordinate system



Local $(\hat{x}, \hat{y}, \hat{z})$ and global (x, y, z) coordinate systems

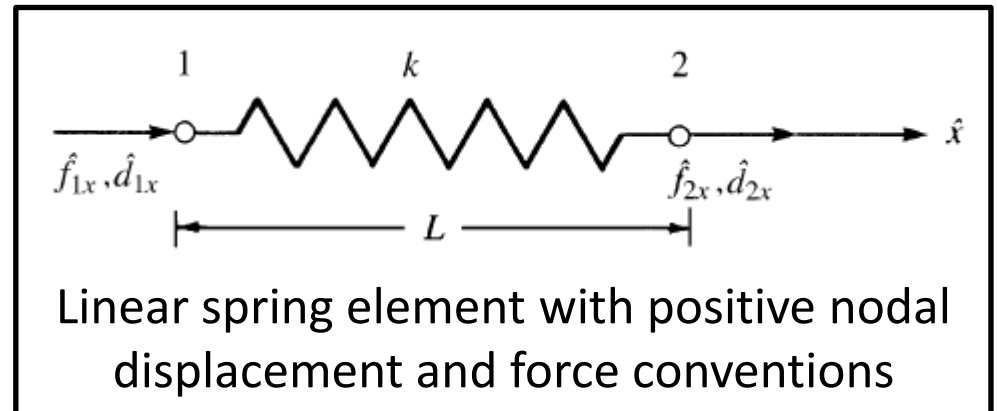
Introduction to the Stiffness (Displacement) Method

Derivation of the Stiffness Matrix for a Spring Element

Degrees of freedom:

$$\hat{d}_{1x} \text{ and } \hat{d}_{2x}$$

k : spring constant or
stiffness of the spring



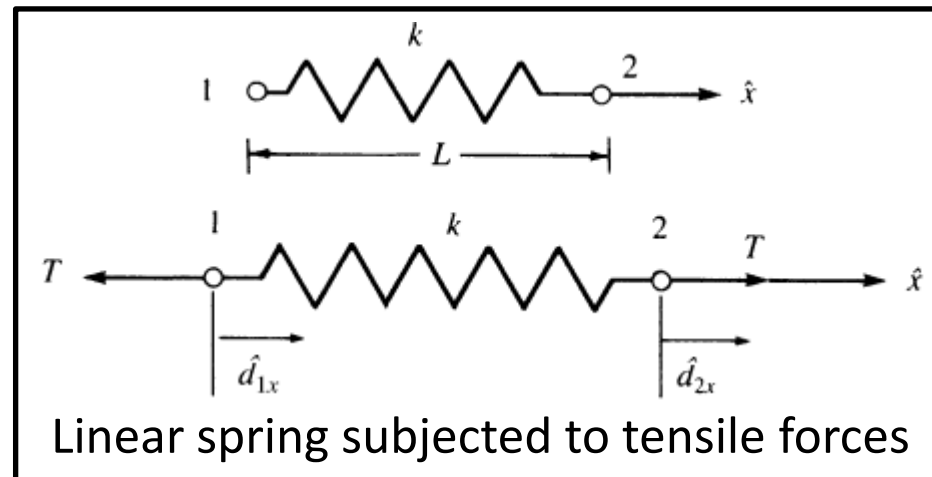
$$\begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{2x} \end{Bmatrix} = \begin{bmatrix} k_{11} & k_{12} \\ k_{21} & k_{22} \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix}$$

We now use the general steps to derive the stiffness matrix for the spring element

Introduction to the Stiffness (Displacement) Method

Derivation of the Stiffness Matrix for a Spring Element

Step 1 Select the Element Type



Consider the *linear spring element* subjected to resulting nodal tensile forces directed along the spring axial direction, so as to be in equilibrium.

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Derivation of the Stiffness Matrix for a Spring Element

Step 2 Select a Displacement Function

$$\hat{u} = a_1 + a_2 \hat{x} \quad \rightarrow \quad \hat{u} = [1 \quad \hat{x}] \begin{Bmatrix} a_1 \\ a_2 \end{Bmatrix}$$

$$\hat{u}(0) = \hat{d}_{1x} = a_1$$

$$\hat{u}(L) = \hat{d}_{2x} = a_2 L + \hat{d}_{1x}$$

$$a_2 = \frac{\hat{d}_{2x} - \hat{d}_{1x}}{L}$$

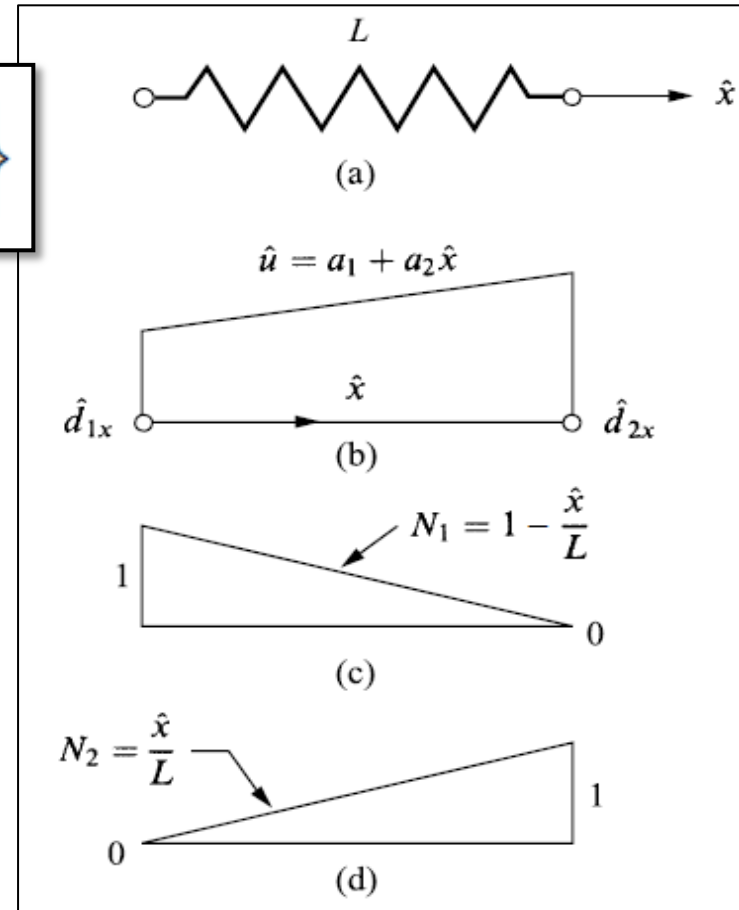
$$\hat{u} = \left(\frac{\hat{d}_{2x} - \hat{d}_{1x}}{L} \right) \hat{x} + \hat{d}_{1x}$$

$$\hat{u} = \begin{bmatrix} 1 - \frac{\hat{x}}{L} & \frac{\hat{x}}{L} \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix}$$

$$\hat{u} = [N_1 \quad N_2] \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix}$$

$$N_1 = 1 - \frac{\hat{x}}{L} \quad \text{and} \quad N_2 = \frac{\hat{x}}{L}$$

**shape functions (or)
Interpolation functions**



Introduction to the Stiffness (Displacement) Method

Derivation of the Stiffness Matrix for a Spring Element

Step 3 Define the Strain/Displacement and Stress/Strain Relationships

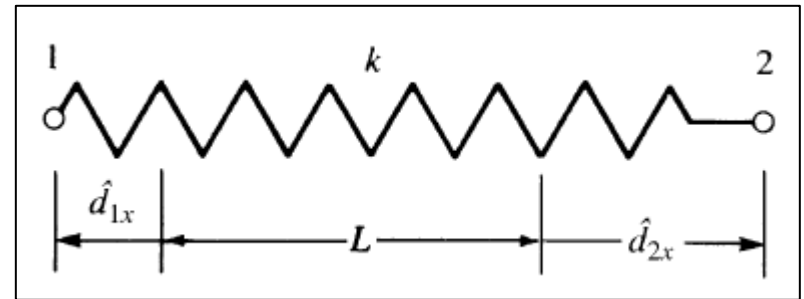
• Due to the tensile force T , the deformation (total elongation) of the spring:

$$\delta = \hat{u}(L) - \hat{u}(0) = \hat{d}_{2x} - \hat{d}_{1x}$$

• Force/deformation relationship:

$$T = k\delta$$

$$T = k(\hat{d}_{2x} - \hat{d}_{1x})$$



Deformed spring

Introduction to the Stiffness (Displacement) Method

Derivation of the Stiffness Matrix for a Spring Element

Step 4 Derive the Element Stiffness Matrix and Equations

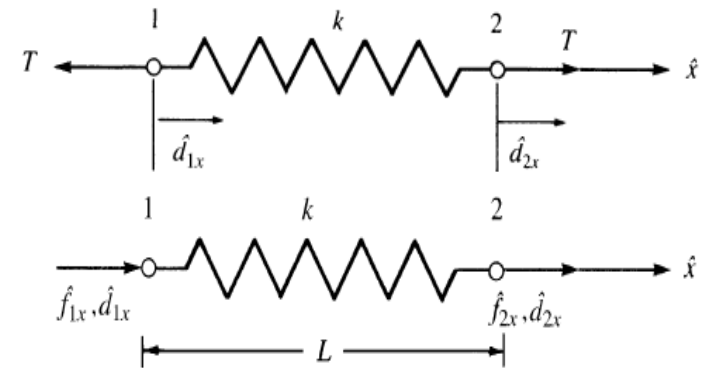
- By the sign convention for nodal forces and equilibrium,

$$\hat{f}_{1x} = -T \quad \hat{f}_{2x} = T$$

$$T = -\hat{f}_{1x} = k(\hat{d}_{2x} - \hat{d}_{1x}) \quad \hat{f}_{1x} = k(\hat{d}_{1x} - \hat{d}_{2x})$$

$$T = \hat{f}_{2x} = k(\hat{d}_{2x} - \hat{d}_{1x}) \quad \hat{f}_{2x} = k(\hat{d}_{2x} - \hat{d}_{1x})$$

$$\begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{2x} \end{Bmatrix} = \begin{bmatrix} k & -k \\ -k & k \end{bmatrix} \begin{Bmatrix} \hat{d}_{1x} \\ \hat{d}_{2x} \end{Bmatrix}$$



**Local stiffness
matrix**

$$\underline{\hat{k}} = \begin{bmatrix} k & -k \\ -k & k \end{bmatrix}$$

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Derivation of the Stiffness Matrix for a Spring Element

Step 5 Assemble the Element Equations to Obtain the Global Equations and Introduce Boundary Conditions

Global stiffness matrix

$$\underline{K} = [K] = \sum_{e=1}^N \underline{k}^{(e)}$$

Global force matrix

$$\underline{F} = \{F\} = \sum_{e=1}^N \underline{f}^{(e)}$$

where \underline{k} and \underline{f} are now element stiffness and force matrices expressed in a global reference frame.

Note: The element matrices must be assembled properly according to the direct stiffness method

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Derivation of the Stiffness Matrix for a Spring Element

Step 6 Solve for the Nodal Displacements

- The displacements are then determined by imposing boundary conditions, such as support conditions, and solving a system of equations, $\underline{F} = \underline{K}\underline{d}$, simultaneously.

Step 7 Solve for the Element Forces

- Finally, the element forces are determined by back-substitution, applied to each element, into equations similar to,

$$\hat{f}_{1x} = k(\hat{d}_{1x} - \hat{d}_{2x})$$

$$\hat{f}_{2x} = k(\hat{d}_{2x} - \hat{d}_{1x})$$

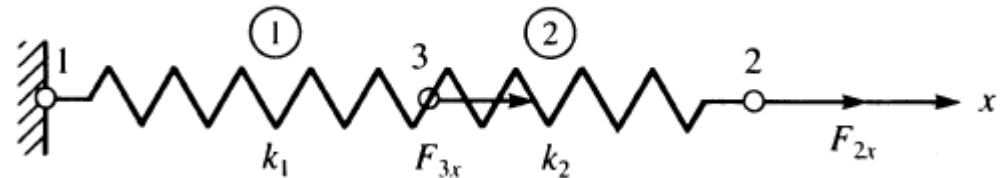
Introduction to the Stiffness (Displacement) Method

Example of a Spring Assemblage

DIRECT EQUILIBRIUM
APPROACH



TOTAL STIFFNESS MATRIX



Element 1

$$\begin{Bmatrix} f_{1x} \\ f_{3x} \end{Bmatrix} = \begin{bmatrix} k_1 & -k_1 \\ -k_1 & k_1 \end{bmatrix} \begin{Bmatrix} d_{1x}^{(1)} \\ d_{3x}^{(1)} \end{Bmatrix}$$

Element 2

$$\begin{Bmatrix} f_{3x} \\ f_{2x} \end{Bmatrix} = \begin{bmatrix} k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \begin{Bmatrix} d_{3x}^{(2)} \\ d_{2x}^{(2)} \end{Bmatrix}$$

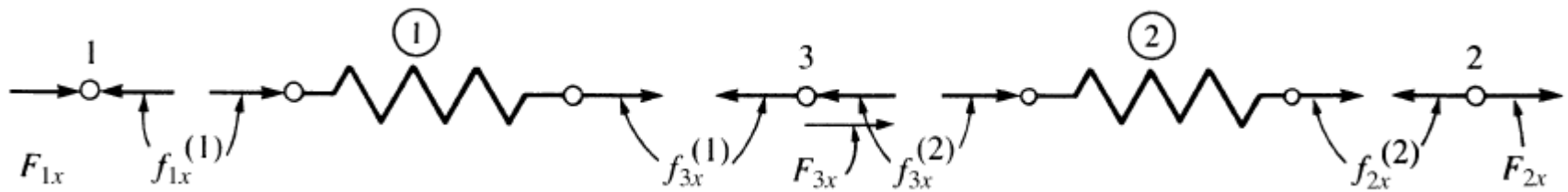
Continuity Or
Compatibility Requirement



$$d_{3x}^{(1)} = d_{3x}^{(2)} = d_{3x}$$

Introduction to the Stiffness (Displacement) Method

Example of a Spring Assemblage



Free-body diagrams of
each element and node

Note: nodal forces consistent with
element force sign convention

Nodal Equilibrium
Equations

$$F_{3x} = f_{3x}^{(1)} + f_{3x}^{(2)}$$

$$F_{2x} = f_{2x}^{(2)}$$

$$F_{1x} = f_{1x}^{(1)}$$



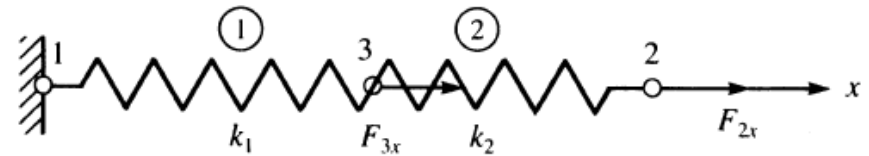
$$F_{3x} = (-k_1 d_{1x} + k_1 d_{3x}) + (k_2 d_{3x} - k_2 d_{2x})$$

$$F_{2x} = -k_2 d_{3x} + k_2 d_{2x}$$

$$F_{1x} = k_1 d_{1x} - k_1 d_{3x}$$

Introduction to the Stiffness (Displacement) Method

Example of a Spring Assemblage



Global Stiffness Equation:

$$\begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \end{Bmatrix} = \begin{bmatrix} k_1 & 0 & -k_1 \\ 0 & k_2 & -k_2 \\ -k_1 & -k_2 & k_1 + k_2 \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{2x} \\ d_{3x} \end{Bmatrix}$$

$$\underline{F} = \underline{K} \underline{d}$$

$$\underline{F} = \begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \end{Bmatrix}$$

$$\underline{K} = \begin{bmatrix} k_1 & 0 & -k_1 \\ 0 & k_2 & -k_2 \\ -k_1 & -k_2 & k_1 + k_2 \end{bmatrix}$$

$$\underline{d} = \begin{Bmatrix} d_{1x} \\ d_{2x} \\ d_{3x} \end{Bmatrix}$$

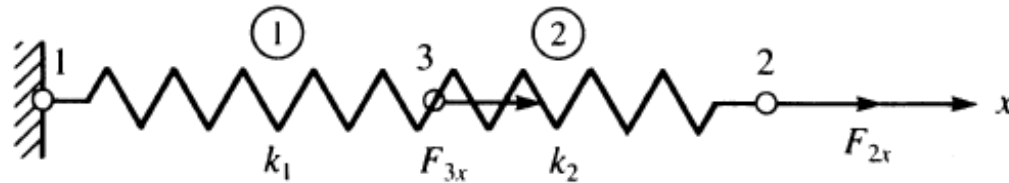
Global Nodal
Force Matrix

Total or Global or System
Stiffness Matrix

Global Nodal
Displacement Matrix

Introduction to the Stiffness (Displacement) Method

Assembling the Total Stiffness Matrix by Superposition (Direct Stiffness Method)



$$\underline{k}^{(1)} = \begin{bmatrix} d_{1x} & d_{3x} \\ k_1 & -k_1 \\ -k_1 & k_1 \end{bmatrix} \begin{matrix} d_{1x} \\ d_{3x} \end{matrix}$$

$$\underline{k}^{(2)} = \begin{bmatrix} d_{3x} & d_{2x} \\ k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \begin{matrix} d_{3x} \\ d_{2x} \end{matrix}$$

$$k_1 \begin{bmatrix} d_{1x} & d_{2x} & d_{3x} \\ 1 & 0 & -1 \\ 0 & 0 & 0 \\ -1 & 0 & 1 \end{bmatrix} \begin{Bmatrix} d_{1x}^{(1)} \\ d_{2x}^{(1)} \\ d_{3x}^{(1)} \end{Bmatrix} = \begin{Bmatrix} f_{1x}^{(1)} \\ f_{2x}^{(1)} \\ f_{3x}^{(1)} \end{Bmatrix}$$

$$k_2 \begin{bmatrix} d_{1x} & d_{2x} & d_{3x} \\ 0 & 0 & 0 \\ 0 & 1 & -1 \\ 0 & -1 & 1 \end{bmatrix} \begin{Bmatrix} d_{1x}^{(2)} \\ d_{2x}^{(2)} \\ d_{3x}^{(2)} \end{Bmatrix} = \begin{Bmatrix} f_{1x}^{(2)} \\ f_{2x}^{(2)} \\ f_{3x}^{(2)} \end{Bmatrix}$$

Introduction to the Stiffness (Displacement) Method

Assembling the Total Stiffness Matrix by Superposition (Direct Stiffness Method)

$$\begin{Bmatrix} f_{1x}^{(1)} \\ 0 \\ f_{3x}^{(1)} \end{Bmatrix} + \begin{Bmatrix} 0 \\ f_{2x}^{(2)} \\ f_{3x}^{(2)} \end{Bmatrix} = \begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \end{Bmatrix} \quad \text{Force Equilibrium at Each Node}$$

$$k_1 \begin{bmatrix} 1 & 0 & -1 \\ 0 & 0 & 0 \\ -1 & 0 & 1 \end{bmatrix} \begin{Bmatrix} d_{1x}^{(1)} \\ d_{2x}^{(1)} \\ d_{3x}^{(1)} \end{Bmatrix} + k_2 \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1 & -1 \\ 0 & -1 & 1 \end{bmatrix} \begin{Bmatrix} d_{1x}^{(2)} \\ d_{2x}^{(2)} \\ d_{3x}^{(2)} \end{Bmatrix} = \begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \end{Bmatrix}$$

$$\boxed{\begin{bmatrix} k_1 & 0 & -k_1 \\ 0 & k_2 & -k_2 \\ -k_1 & -k_2 & k_1 + k_2 \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{2x} \\ d_{3x} \end{Bmatrix} = \begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \end{Bmatrix}}$$

Introduction to the Stiffness (Displacement) Method

Assembling the Total Stiffness Matrix by Superposition (Direct Stiffness Method)

Direct, or Short-cut, Form of the Direct Stiffness Method

$$\underline{k}^{(1)} = \begin{array}{cc} d_{1x} & d_{3x} \\ \left[\begin{array}{cc} k_1 & -k_1 \\ -k_1 & k_1 \end{array} \right] & \begin{array}{l} d_{1x} \\ d_{3x} \end{array} \end{array} \quad \longleftrightarrow \quad \underline{k}^{(2)} = \begin{array}{cc} d_{3x} & d_{2x} \\ \left[\begin{array}{cc} k_2 & -k_2 \\ -k_2 & k_2 \end{array} \right] & \begin{array}{l} d_{3x} \\ d_{2x} \end{array} \end{array}$$

$$\underline{K} = \begin{array}{ccc} d_{1x} & d_{2x} & d_{3x} \\ \left[\begin{array}{ccc} k_1 & 0 & -k_1 \\ 0 & k_2 & -k_2 \\ -k_1 & -k_2 & k_1 + k_2 \end{array} \right] & \begin{array}{l} d_{1x} \\ d_{2x} \\ d_{3x} \end{array} \end{array}$$

Introduction to the Stiffness (Displacement) Method

Boundary Conditions (BCs)

- Without specifying boundary conditions:
 - Mathematically: \underline{K} is singular, its determinant will be zero, and its inverse will not exist
 - Physically: the structural system is unstable, free to move as a rigid body and not resist any applied loads
- Boundary conditions are of two general types:
 - Homogeneous BCs, occur at locations that are completely prevented from movement
 - Nonhomogeneous BCs, occur where finite nonzero values of displacement are specified, such as the settlement of a support.

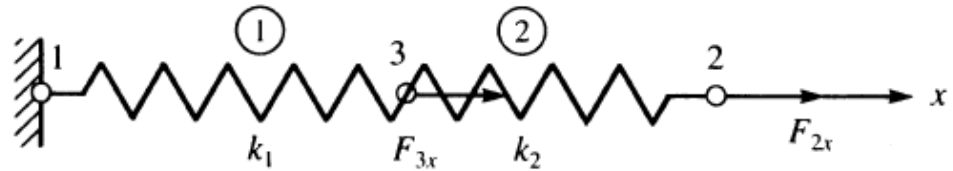
Introduction to the Stiffness (Displacement) Method

Boundary Conditions

**Homogeneous
Boundary Conditions**

$$d_{1x} = 0$$

Node 1 is fixed



$$\begin{bmatrix} k_1 & 0 & -k_1 \\ 0 & k_2 & -k_2 \\ -k_1 & -k_2 & k_1 + k_2 \end{bmatrix} \begin{Bmatrix} 0 \\ d_{2x} \\ d_{3x} \end{Bmatrix} = \begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \end{Bmatrix}$$

$$k_1(0) + (0)d_{2x} - k_1d_{3x} = F_{1x} \longrightarrow \text{Unknown Reaction}$$

$$0(0) + k_2d_{2x} - k_2d_{3x} = F_{2x} \quad \left. \begin{array}{l} \\ \end{array} \right\} \longrightarrow \text{Known Applied Loads}$$

$$-k_1(0) - k_2d_{2x} + (k_1 + k_2)d_{3x} = F_{3x}$$

Introduction to the Stiffness (Displacement) Method

Boundary Conditions

- Delete the rows and columns corresponding to the zero-displacement degrees of freedom from the original set of equations,

$$\begin{bmatrix} k_2 & -k_2 \\ -k_2 & k_1 + k_2 \end{bmatrix} \begin{Bmatrix} d_{2x} \\ d_{3x} \end{Bmatrix} = \begin{Bmatrix} F_{2x} \\ F_{3x} \end{Bmatrix}$$

- Then solve for the unknown displacements and the reaction,

$$\begin{Bmatrix} d_{2x} \\ d_{3x} \end{Bmatrix} = \begin{bmatrix} k_2 & -k_2 \\ -k_2 & k_1 + k_2 \end{bmatrix}^{-1} \begin{Bmatrix} F_{2x} \\ F_{3x} \end{Bmatrix} = \begin{bmatrix} \frac{1}{k_2} + \frac{1}{k_1} & \frac{1}{k_1} \\ \frac{1}{k_1} & \frac{1}{k_1} \end{bmatrix} \begin{Bmatrix} F_{2x} \\ F_{3x} \end{Bmatrix}$$

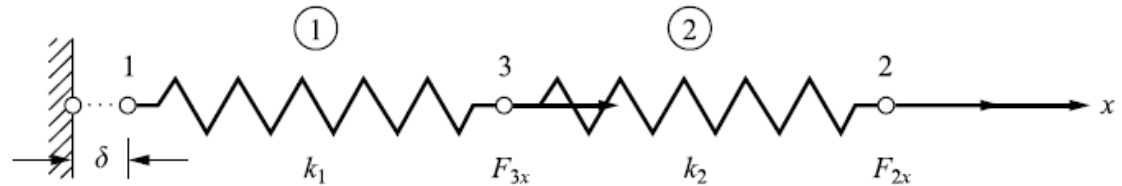
$$F_{1x} = -k_1 d_{3x} = -F_{2x} - F_{3x}$$

Note: for matrix inverse, review Appendix A, Page 716

Introduction to the Stiffness (Displacement) Method

Boundary Conditions

**Nonhomogeneous
Boundary Conditions**



$$d_{1x} = \delta$$

**Known displacement
at node 1**

$$\begin{bmatrix} k_1 & 0 & -k_1 \\ 0 & k_2 & -k_2 \\ -k_1 & -k_2 & k_1 + k_2 \end{bmatrix} \begin{Bmatrix} \delta \\ d_{2x} \\ d_{3x} \end{Bmatrix} = \begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \end{Bmatrix}$$

$$k_1 \delta + 0d_{2x} - k_1 d_{3x} = F_{1x} \quad \longrightarrow \quad \text{Unknown Reaction}$$

$$0\delta + k_2 d_{2x} - k_2 d_{3x} = F_{2x} \quad \left. \begin{array}{l} \longrightarrow \\ \longrightarrow \end{array} \right\} \quad \text{Known Applied Loads}$$

$$-k_1 \delta - k_2 d_{2x} + (k_1 + k_2) d_{3x} = F_{3x}$$

Introduction to the Stiffness (Displacement) Method

Boundary Conditions

- Transform the terms associated with the known displacements to the right-side force matrix before solving for the unknown nodal displacements.

$$k_2 d_{2x} - k_2 d_{3x} = F_{2x}$$

$$-k_2 d_{2x} + (k_1 + k_2) d_{3x} = +k_1 \delta + F_{3x}$$

- Then solve for the unknown displacements and the reaction,

$$\begin{bmatrix} k_2 & -k_2 \\ -k_2 & k_1 + k_2 \end{bmatrix} \begin{Bmatrix} d_{2x} \\ d_{3x} \end{Bmatrix} = \begin{Bmatrix} F_{2x} \\ k_1 \delta + F_{3x} \end{Bmatrix}$$

$$F_{1x} = k_1 \delta - k_1 d_{3x}$$

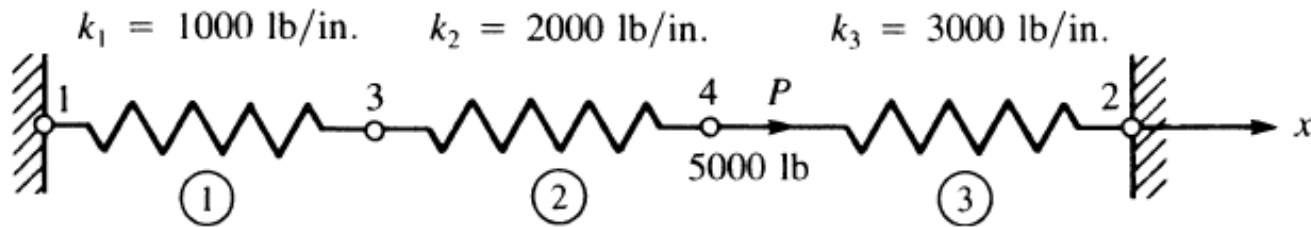
Introduction to the Stiffness (Displacement) Method

Boundary Conditions

- Properties of the stiffness matrix:
 - \underline{K} is symmetric, as is each of the element stiffness matrices
 - \underline{K} is singular, and thus no inverse exists until sufficient BCs are imposed to remove the singularity and prevent rigid body motion.
 - the main diagonal terms of \underline{K} are always positive.

Introduction to the Stiffness (Displacement) Method

Example 1



- Nodes 1 and 2 are fixed
- A force of 5000 lb is applied at node 4 in the x direction.

Obtain:

- (a) The global stiffness matrix
- (b) The displacements of nodes 3 and 4
- (c) The reaction forces at nodes 1 and 2
- (d) The forces in each spring

Introduction to the Stiffness (Displacement) Method

Example 1

(a) The global stiffness matrix

Element Stiffness Matrix

$$\underline{k}^{(1)} = \begin{matrix} & \begin{matrix} 1 & 3 \end{matrix} \\ \begin{bmatrix} 1000 & -1000 \\ -1000 & 1000 \end{bmatrix} & \begin{matrix} 1 \\ 3 \end{matrix} \end{matrix} \quad \underline{k}^{(2)} = \begin{matrix} & \begin{matrix} 3 & 4 \end{matrix} \\ \begin{bmatrix} 2000 & -2000 \\ -2000 & 2000 \end{bmatrix} & \begin{matrix} 3 \\ 4 \end{matrix} \end{matrix} \quad \underline{k}^{(3)} = \begin{matrix} & \begin{matrix} 4 & 2 \end{matrix} \\ \begin{bmatrix} 3000 & -3000 \\ -3000 & 3000 \end{bmatrix} & \begin{matrix} 4 \\ 2 \end{matrix} \end{matrix}$$

- Using the concept of superposition (the direct stiffness method), we obtain the global stiffness matrix as

$$\underline{K} = \underline{k}^{(1)} + \underline{k}^{(2)} + \underline{k}^{(3)} \quad \underline{K} = \begin{matrix} & \begin{matrix} 1 & 2 & 3 & 4 \end{matrix} \\ \begin{bmatrix} 1000 & 0 & -1000 & 0 \\ 0 & 3000 & 0 & -3000 \\ -1000 & 0 & 1000 + 2000 & -2000 \\ 0 & -3000 & -2000 & 2000 + 3000 \end{bmatrix} & \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \end{matrix} \end{matrix}$$

Introduction to the Stiffness (Displacement) Method

Example 1

(b) The displacements of nodes 3 and 4

Global Stiffness Equation

$$\begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \\ F_{4x} \end{Bmatrix} = \begin{bmatrix} 1000 & 0 & -1000 & 0 \\ 0 & 3000 & 0 & -3000 \\ -1000 & 0 & 3000 & -2000 \\ 0 & -3000 & -2000 & 5000 \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{2x} \\ d_{3x} \\ d_{4x} \end{Bmatrix}$$

Homogeneous Boundary Conditions: $d_{1x} = 0$ and $d_{2x} = 0$

$$\begin{Bmatrix} F_{3x} \\ F_{4x} \end{Bmatrix} = \begin{bmatrix} 3000 & -2000 \\ -2000 & 5000 \end{bmatrix} \begin{Bmatrix} d_{3x} \\ d_{4x} \end{Bmatrix}$$

Global nodal displacements: $d_{3x} = \frac{10}{11}$ in. $d_{4x} = \frac{15}{11}$ in.

Introduction to the Stiffness (Displacement) Method

Example 1

(c) The reaction forces at nodes 1 and 2

$$\begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \\ F_{4x} \end{Bmatrix} = \begin{bmatrix} 1000 & 0 & -1000 & 0 \\ 0 & 3000 & 0 & -3000 \\ -1000 & 0 & 3000 & -2000 \\ 0 & -3000 & -2000 & 5000 \end{bmatrix} \begin{Bmatrix} 0 \\ 0 \\ \frac{10}{11} \\ \frac{15}{11} \end{Bmatrix}$$

$$F_{1x} = \frac{-10,000}{11} \text{ lb}$$

$$F_{2x} = \frac{-45,000}{11} \text{ lb}$$

$$F_{3x} = 0$$

$$F_{4x} = 5000 \text{ lb}$$

The sum of the reactions F_{1x} and F_{2x} is equal in magnitude but opposite in direction to the applied force F_{4x} .

This result verifies equilibrium of the whole spring assemblage.

Introduction to the Stiffness (Displacement) Method

(d) The forces in each spring

Example 1

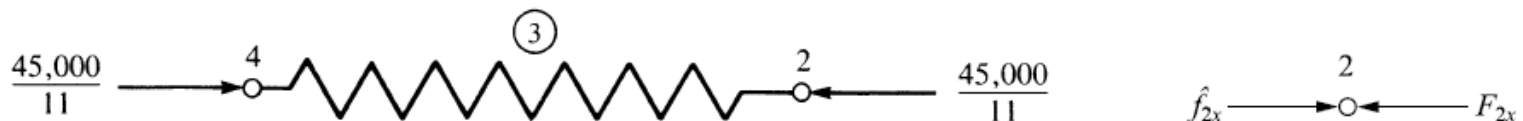
Element 1 $\begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{3x} \end{Bmatrix} = \begin{bmatrix} 1000 & -1000 \\ -1000 & 1000 \end{bmatrix} \begin{Bmatrix} 0 \\ \frac{10}{11} \end{Bmatrix}$ $\hat{f}_{1x} = \frac{-10,000}{11} \text{ lb}$ $\hat{f}_{3x} = \frac{10,000}{11} \text{ lb}$



Element 2 $\begin{Bmatrix} \hat{f}_{3x} \\ \hat{f}_{4x} \end{Bmatrix} = \begin{bmatrix} 2000 & -2000 \\ -2000 & 2000 \end{bmatrix} \begin{Bmatrix} \frac{10}{11} \\ \frac{15}{11} \end{Bmatrix}$ $\hat{f}_{3x} = \frac{-10,000}{11} \text{ lb}$ $\hat{f}_{4x} = \frac{10,000}{11} \text{ lb}$

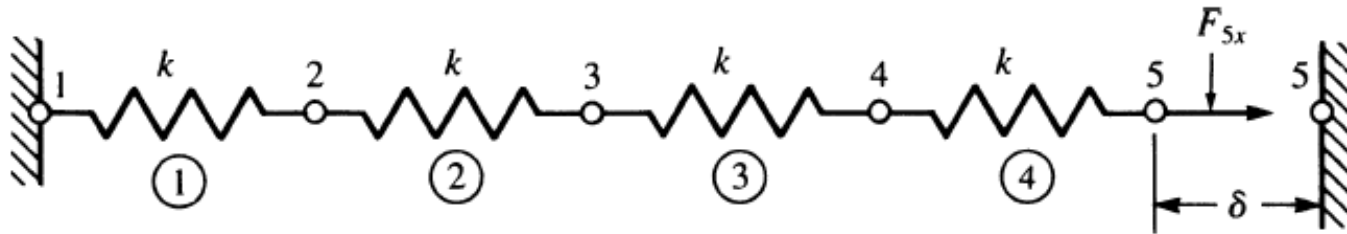


Element 3 $\begin{Bmatrix} \hat{f}_{4x} \\ \hat{f}_{2x} \end{Bmatrix} = \begin{bmatrix} 3000 & -3000 \\ -3000 & 3000 \end{bmatrix} \begin{Bmatrix} \frac{15}{11} \\ 0 \end{Bmatrix}$ $\hat{f}_{4x} = \frac{45,000}{11} \text{ lb}$ $\hat{f}_{2x} = \frac{-45,000}{11} \text{ lb}$



Introduction to the Stiffness (Displacement) Method

Example 2



- Node 1 is fixed
- Node 5 is given a fixed, known displacement $d \delta = 20$ mm.
- The spring constants are all equal to $k = 200$ kN/m.
- **Obtain:**
 - (a) The global stiffness matrix
 - (b) The displacements of nodes 2 and 4
 - (c) The global nodal forces
 - (d) The local element forces

Introduction to the Stiffness (Displacement) Method

(a) The global stiffness matrix

Example 2

**Element
Stiffness Matrix**

$$\underline{k}^{(1)} = \underline{k}^{(2)} = \underline{k}^{(3)} = \underline{k}^{(4)} = \begin{bmatrix} 200 & -200 \\ -200 & 200 \end{bmatrix}$$

**Global
Stiffness Matrix**

$$\underline{K} = \begin{bmatrix} 200 & -200 & 0 & 0 & 0 \\ -200 & 400 & -200 & 0 & 0 \\ 0 & -200 & 400 & -200 & 0 \\ 0 & 0 & -200 & 400 & -200 \\ 0 & 0 & 0 & -200 & 200 \end{bmatrix} \frac{\text{kN}}{\text{m}}$$

Introduction to the Stiffness (Displacement) Method

(b) The displacements of nodes 2 and 4

Example 2

$$\begin{Bmatrix} F_{1x} \\ F_{2x} \\ F_{3x} \\ F_{4x} \\ F_{5x} \end{Bmatrix} = \begin{bmatrix} 200 & -200 & 0 & 0 & 0 \\ -200 & 400 & -200 & 0 & 0 \\ 0 & -200 & 400 & -200 & 0 \\ 0 & 0 & -200 & 400 & -200 \\ 0 & 0 & 0 & -200 & 200 \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{2x} \\ d_{3x} \\ d_{4x} \\ d_{5x} \end{Bmatrix}$$

$$d_{1x} = 0 \text{ and } d_{5x} = 20 \text{ mm}$$

$$F_{2x} = 0, F_{3x} = 0, \text{ and } F_{4x} = 0$$

$$\begin{Bmatrix} 0 \\ 0 \\ 0 \end{Bmatrix} = \begin{bmatrix} -200 & 400 & -200 & 0 & 0 \\ 0 & -200 & 400 & -200 & 0 \\ 0 & 0 & -200 & 400 & -200 \end{bmatrix} \begin{Bmatrix} 0 \\ d_{2x} \\ d_{3x} \\ d_{4x} \\ 0.02 \text{ m} \end{Bmatrix}$$

Transposing the product of the appropriate stiffness coefficient (-200) multiplied by the known displacement (0.02m) to the left side.

$$\begin{Bmatrix} 0 \\ 0 \\ 4 \text{ kN} \end{Bmatrix} = \begin{bmatrix} 400 & -200 & 0 \\ -200 & 400 & -200 \\ 0 & -200 & 400 \end{bmatrix} \begin{Bmatrix} d_{2x} \\ d_{3x} \\ d_{4x} \end{Bmatrix}$$

$$d_{2x} = 0.005 \text{ m}$$

$$d_{3x} = 0.01 \text{ m}$$

$$d_{4x} = 0.015 \text{ m}$$

Introduction to the Stiffness (Displacement) Method

(c) The global nodal forces

Example 2

$$F_{1x} = (-200)(0.005) = -1.0 \text{ kN}$$

$$F_{2x} = (400)(0.005) - (200)(0.01) = 0$$

$$F_{3x} = (-200)(0.005) + (400)(0.01) - (200)(0.015) = 0$$

$$F_{4x} = (-200)(0.01) + (400)(0.015) - (200)(0.02) = 0$$

$$F_{5x} = (-200)(0.015) + (200)(0.02) = 1.0 \text{ kN}$$

Introduction to the Stiffness (Displacement) Method

(d) The local element forces

Example 2

Element 1

$$\begin{Bmatrix} \hat{f}_{1x} \\ \hat{f}_{2x} \end{Bmatrix} = \begin{bmatrix} 200 & -200 \\ -200 & 200 \end{bmatrix} \begin{Bmatrix} 0 \\ 0.005 \end{Bmatrix}$$

$$\hat{f}_{1x} = -1.0 \text{ kN} \quad \hat{f}_{2x} = 1.0 \text{ kN}$$

Element 3

$$\begin{Bmatrix} \hat{f}_{3x} \\ \hat{f}_{4x} \end{Bmatrix} = \begin{bmatrix} 200 & -200 \\ -200 & 200 \end{bmatrix} \begin{Bmatrix} 0.01 \\ 0.015 \end{Bmatrix}$$

$$\hat{f}_{3x} = -1 \text{ kN} \quad \hat{f}_{4x} = 1 \text{ kN}$$

Element 2

$$\begin{Bmatrix} \hat{f}_{2x} \\ \hat{f}_{3x} \end{Bmatrix} = \begin{bmatrix} 200 & -200 \\ -200 & 200 \end{bmatrix} \begin{Bmatrix} 0.005 \\ 0.01 \end{Bmatrix}$$

$$\hat{f}_{2x} = -1 \text{ kN} \quad \hat{f}_{3x} = 1 \text{ kN}$$

Element 4

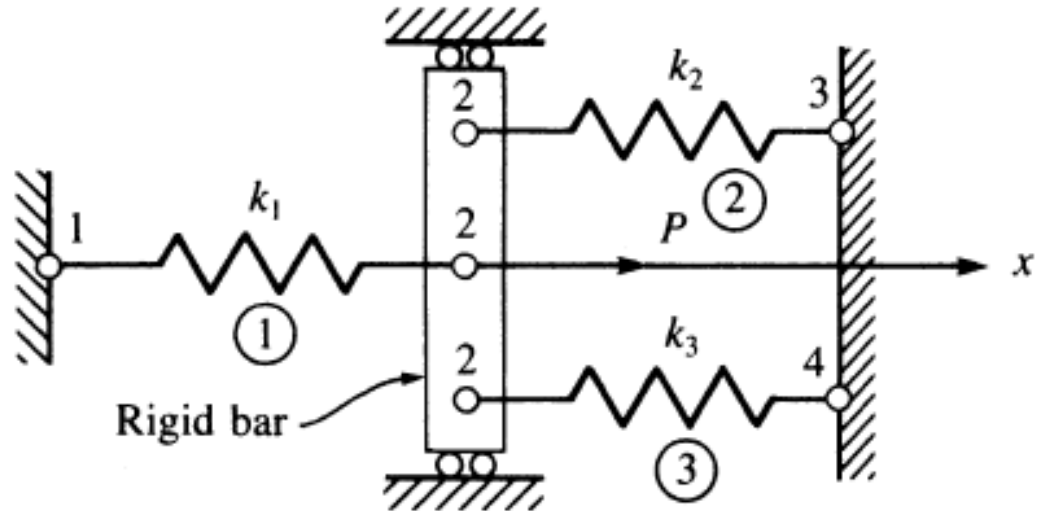
$$\begin{Bmatrix} \hat{f}_{4x} \\ \hat{f}_{5x} \end{Bmatrix} = \begin{bmatrix} 200 & -200 \\ -200 & 200 \end{bmatrix} \begin{Bmatrix} 0.015 \\ 0.02 \end{Bmatrix}$$

$$\hat{f}_{4x} = -1 \text{ kN} \quad \hat{f}_{5x} = 1 \text{ kN}$$

Introduction to the Stiffness (Displacement) Method

Example 3

P is an applied force at node 2



- Formulate the global stiffness matrix and equations for solution of the unknown global displacement and forces.
 - a) Using the direct equilibrium approach
 - b) Using the direct stiffness method

Introduction to the Stiffness (Displacement) Method

Example 3

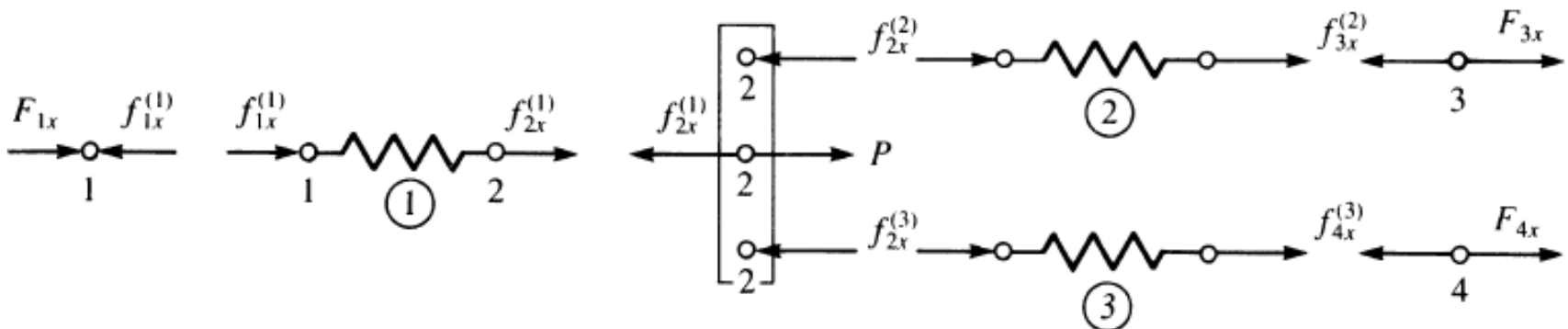
a) Using the direct equilibrium approach

- The boundary conditions: $d_{1x} = 0$ $d_{3x} = 0$ $d_{4x} = 0$
- The compatibility condition at node 2 is, $d_{2x}^{(1)} = d_{2x}^{(2)} = d_{2x}^{(3)} = d_{2x}$
- The nodal equilibrium conditions are,

$$F_{1x} = f_{1x}^{(1)} \qquad F_{3x} = f_{3x}^{(2)}$$

$$P = f_{2x}^{(1)} + f_{2x}^{(2)} + f_{2x}^{(3)} \qquad F_{4x} = f_{4x}^{(3)}$$

- The element and nodal force free-body diagrams,



Introduction to the Stiffness (Displacement) Method

Example 3

a) Using the direct equilibrium approach

- The total or global equilibrium equations,

$$F_{1x} = k_1 d_{1x} - k_1 d_{2x}$$

$$P = -k_1 d_{1x} + k_1 d_{2x} + k_2 d_{2x} - k_2 d_{3x} + k_3 d_{2x} - k_3 d_{4x}$$

$$F_{3x} = -k_2 d_{2x} + k_2 d_{3x}$$

$$F_{4x} = -k_3 d_{2x} + k_3 d_{4x}$$

**Global Stiffness
Matrix**



$$\begin{Bmatrix} F_{1x} \\ P \\ F_{3x} \\ F_{4x} \end{Bmatrix} = \begin{bmatrix} k_1 & -k_1 & 0 & 0 \\ -k_1 & k_1 + k_2 + k_3 & -k_2 & -k_3 \\ 0 & -k_2 & k_2 & 0 \\ 0 & -k_3 & 0 & k_3 \end{bmatrix} \begin{Bmatrix} d_{1x} \\ d_{2x} \\ d_{3x} \\ d_{4x} \end{Bmatrix}$$

$$d_{2x} = \frac{P}{k_1 + k_2 + k_3}$$

$$F_{1x} = -k_1 d_{2x}$$

$$F_{3x} = -k_2 d_{2x}$$

$$F_{4x} = -k_3 d_{2x}$$

Introduction to the Stiffness (Displacement) Method

Example 3

a) Using the direct stiffness method

$$\underline{k}^{(1)} = \begin{matrix} & d_{1x} & d_{2x} \\ \begin{bmatrix} k_1 & -k_1 \\ -k_1 & k_1 \end{bmatrix} \end{matrix} \quad \underline{k}^{(2)} = \begin{matrix} & d_{2x} & d_{3x} \\ \begin{bmatrix} k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \end{matrix} \quad \underline{k}^{(3)} = \begin{matrix} & d_{2x} & d_{4x} \\ \begin{bmatrix} k_3 & -k_3 \\ -k_3 & k_3 \end{bmatrix} \end{matrix}$$

**Global Stiffness
Matrix**

$$\underline{K} = \begin{matrix} & d_{1x} & d_{2x} & d_{3x} & d_{4x} \\ \begin{bmatrix} k_1 & -k_1 & 0 & 0 \\ -k_1 & k_1 + k_2 + k_3 & -k_2 & -k_3 \\ 0 & -k_2 & k_2 & 0 \\ 0 & -k_3 & 0 & k_3 \end{bmatrix} \end{matrix}$$

Then write the global equilibrium equations and solve for the global forces.