Chapter 7: Internal forces in Frames and Beams

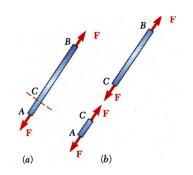
In Chapter 6, we considered internal forces in trusses. We saw that all the members are 2-force members that carry only tension or compression.

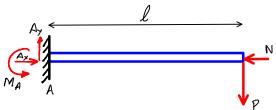
In this chapter, we will consider internal forces in Frames and Beams. Recall that these structures have atleast one multi-force member.

Multi-force members can carry additional types of internal forces such as shear and bending moment in addition to tension/compression.

For example, consider the cantilever beam shown with an end load. We can find the external forces using the FBD of the entire beam.







However we may also want to find out the internal forces (and moments) at different points of the beam. This will help us decide if the beam can support the applied load or not.

To do this, we imagine two (or more) sub-parts of the beam as shown.

$$\leq f_y = 0 \Rightarrow + P - V_x = 0 \Rightarrow V_x = P$$

$$\leq M_A = 0 \Rightarrow +Pl + M_X - V_X x = 0$$

$$\Rightarrow M_X = -Pl + Px$$

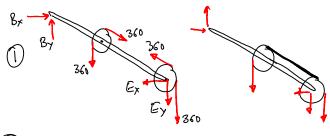
$$M_x = P(x-l)$$

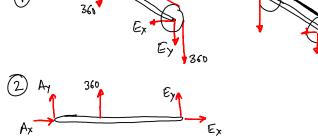
 $\leq M_{x} = 0 \Rightarrow -M_{x} - P(l-x) = 0 \Rightarrow Mx = P(x-l)$

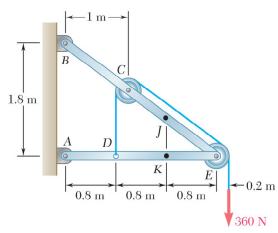
Exercise 7.17 & 7.18

Radius of pulleys = 200 mm

Find the internal forces (& moments) at J & K.







PART-A External

$$\frac{F6D(2)}{4} \stackrel{?}{\Rightarrow} \stackrel{?}{\Rightarrow} A_{x} + E_{x} = 0$$

$$\stackrel{?}{\Rightarrow} F_{y} = 0 \stackrel{?}{\Rightarrow} A_{y} + 360 + E_{y} = 0 \stackrel{?}{\Rightarrow} E_{y} = -120 \text{ N}$$

$$\stackrel{?}{\Rightarrow} M_{E} = 0 \stackrel{?}{\Rightarrow} -A_{y} \times 2.4 - 360 \times 1.6 = 0 \stackrel{?}{\Rightarrow} A_{y} = -360 \times 46 = -240 \text{ N}$$

$$\Rightarrow B_{X} = \frac{360 \times 1.4 - 600 \times 2.4}{1.8} = \frac{-520 \text{N}}{-520 \text{N}} \Rightarrow E_{X} = -520 \text{N}$$

$$\Rightarrow A_{X} = 520 \text{ N}$$

PART-B Internal forces & moments

Take the cut at point I perpendicular to BCE.

To find M, V, N:-

FBD 3: (Rotated co-ordinate axis)

$$\leq F_{x}=0 \Rightarrow B_{x}\cos\theta - B_{y}\sin\theta + 360 + 360 \sin\theta - N = 0$$

$$\stackrel{\Rightarrow}{\neq} F_{y} = 0 \Rightarrow \begin{cases} N = -200 \,\text{N} & (\text{TENSILE}) \\ B_{x} \sin\theta + B_{y} \cos\theta - 360 \cos\theta - V = 0 \end{cases}$$

$$\stackrel{>}{\approx} M_{B} = 0 \qquad \Rightarrow \boxed{V = -120N}$$

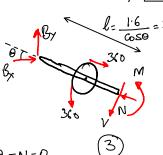
$$\stackrel{>}{\Rightarrow} M - V \times 2 - 360 \times 0.2 - 360 \times 0.8 = 0$$

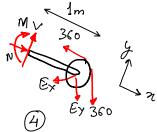
$$\Rightarrow \boxed{M = +120 Nm}$$

FBD (4) (To check)

$$2f_{x} = N - E_{x} \cos \theta + E_{y} \sin \theta + 360 \sin \theta - 360 = 0$$

 $2f_{y} = V - E_{x} \sin \theta - E_{y} \cos \theta - 360 \cos \theta = 0$
 $2f_{y} = V - E_{x} \sin \theta - E_{y} \cos \theta - 360 \cos \theta = 0$
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 $2f_{y} = V - E_{x} \sin \theta - E_{y} \cos \theta - 260 \cos \theta = 0$
 $2f_{y} = V - E_{x} \sin \theta - E_{y} \cos \theta + E_{y} \sin \theta + E_{y} \cos \theta = 0$
 $2f_{y} = V - E_{x} \sin \theta - E_{y} \cos \theta + E_{y} \cos \theta + E_{y} \cos \theta = 0$
 $2f_{y} = V - E_{x} \sin \theta - E_{y} \cos \theta + E_{y} \cos \theta = 0$
 $2f_{y} = V - E_{x} \sin \theta - E_{y} \cos \theta + E_{y} \cos \theta + E_{y} \cos \theta = 0$
 $2f_{y} = V - E_{x} \cos \theta + E_{y} \cos \theta + E$

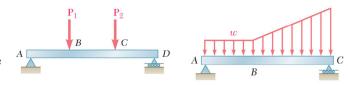




7.3 - 7.4 Internal Forces in Beams

Beams can point or distributed loads acting on them.

Beams may also be externally determinate or indeterminate depending upon the type of support.



Statically Determinate Beams

Statically Indeterminate Beams

Statically Indeterminate Beams

(a) Simply supported beam

(b) Overhanging beam

(c) Cantilever beam

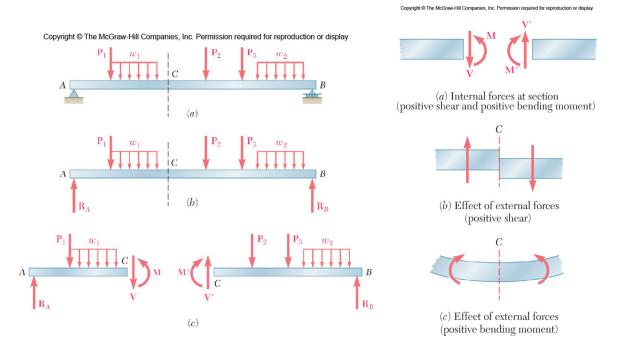
Statically Indeterminate Beams

(e) Beam fixed at one end and simply supported at the other end

Shear and Bending Moment in Beams

Consider the Beam shown carrying some loads. We can find out the reactions \mathbf{R}_A and \mathbf{R}_B for external equilibrium. To find the internal forces, consider the cut shown.

The following convention is adopted for the positive shear and bending moments in beams.



7.5 Shear and Bending Moment Diagrams

Recall the cantilever beam from the previous section.

Nx: Areial force (Tension/Compression)

Vx: SHEAR Force

Mx: BENDING Moment

Using the FBD of individual parts of the beam we found:

$$N_{x} = N$$

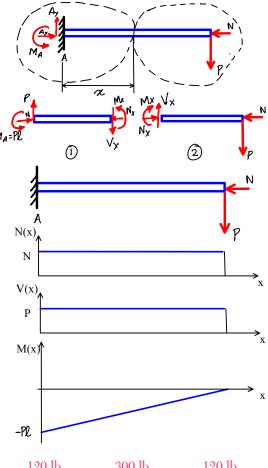
$$M_x = P(x-l)$$

If we plot these INTERNAL forces and moments along the length of the beam, the resulting diagrams are called

Axial force diagram N(x)

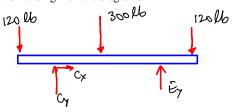
Shear force diagram V(x)

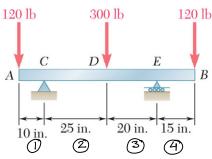
Bending moment diagram M(x)



Exercise 7.38

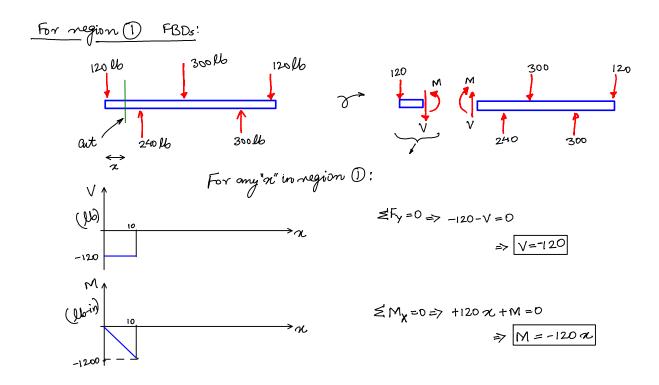
Plot the Shear force and Bending moment diagrams.

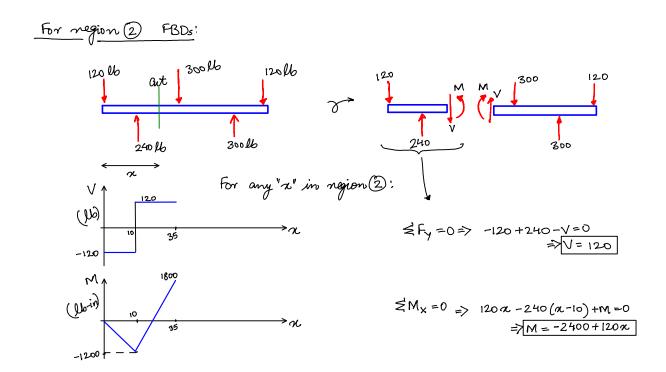


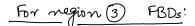


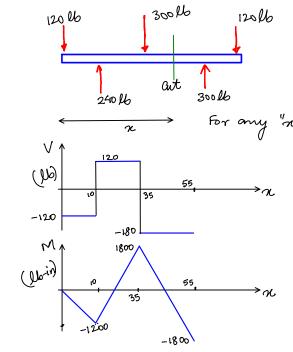
 $\leq f_x = 0 \Rightarrow C_x = 0$

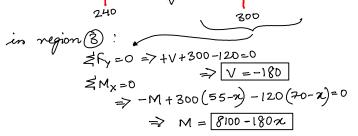
To draw the Shear force & Bending Moment diagrams: - Consider the following "regions" of n along the beam:





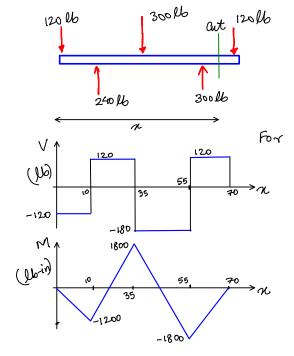


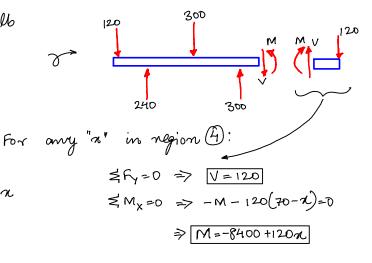




120

For negion (4) FBDs!





Maximum Absolute Value of Shear: 180 lb

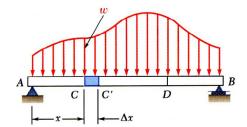
Moment: 1800 lb-in

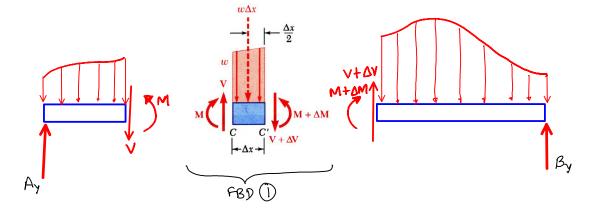
7.6 Load vs. Shear vs. Bending moment

Drawing Shear force and Bending moment diagrams for a beam can be simplified by using relationships between <u>Load vs. Shear</u> and <u>Shear vs. Bending Moment</u>.

These relationships can be derived simply from statics as follows.

Consider a small Δx length of <u>any beam</u> carrying a distributed load.





$$\frac{FBD(0):}{\Rightarrow F_{y}=0} \Rightarrow y' - w\Delta x - (y' + \Delta v) = 0$$

$$\Rightarrow w = -\frac{\Delta V}{\Delta x} \qquad \text{Take } \lim_{\Delta x \to 0} -\frac{\Delta V}{\Delta x} = \Rightarrow w = -\frac{\Delta V}{\partial x}$$

Integrating

$$V_D - V_C = -\int_{x_C}^{x_D} w \, dx = -(\text{area under load curve})$$

$$M_D - M_C = \int_{x_C}^{x_D} V dx =$$
(area under shear curve)

Read examples 7.4, 7.5, 7.6 and 7.7.

Exercise 7.85

Write the expressions of Shear and Bending Moments. Draw the diagrams. Verify the relationships between Load vs. Shear and Shear vs. Bending Moment.

Find the location of the maximum Bending Moment.

$$\omega = -\frac{dV}{d\alpha}$$

$$\Rightarrow V_{x} - V_{A} = -\int_{0}^{x} (\omega_{0} - \underline{\omega}_{0} x) dx$$

$$\underbrace{\text{Note:}}_{0} V_{A} = A_{y} = \underbrace{(\omega_{0} L)}_{2} x_{3}^{2}$$

$$\Rightarrow \sqrt{x = \frac{\omega_0 L}{3} - \omega_0 x + \frac{\omega_0}{L} \frac{\chi^2}{2}}$$

Alternatively: FBD (2):

$$\Rightarrow V + \frac{\omega_0 L}{6} - \frac{\omega_0 (L - \chi)^2}{2} = 0$$

$$\Rightarrow V = -\frac{\omega_0 L}{C} + \frac{\omega_0}{2L} (L^2 - 2L \chi + \chi^2)$$

$$\Rightarrow V = \frac{\omega_0 L}{3} - \omega_0 x + \frac{\omega_0}{L} \frac{\chi^2}{2}$$

$$V = \frac{dM}{d\alpha}$$

$$\Rightarrow M_{x} - M_{A} = \int_{0}^{\infty} \left(\frac{\omega_{o}L}{3} - \omega_{o}x + \frac{\omega_{o}x^{2}}{L} \right) dx$$

$$\Rightarrow M_{x} = \frac{\omega_{o}L}{3}x - \frac{\omega_{o}x^{2}}{2} + \frac{\omega_{o}x^{3}}{L} \xrightarrow{6} **$$

Alternatively from FBD (2):

$$\stackrel{?}{\neq} M_8 = 0 \implies -M_{\mathcal{R}} - V_{\mathcal{R}} (L-\mathcal{R}) + \underbrace{\omega_0}_{L} \underbrace{(L-\mathcal{R})^2}_{2} \times \frac{2}{3} (L-\mathcal{R}) = 0$$

$$\implies M_{\mathcal{R}} = -\left(\underbrace{\omega_0 L}_{3} - \omega_0 \mathcal{R} + \underbrace{\omega_0}_{L} \frac{\mathcal{R}^2}{2}\right) (L-\mathcal{R}) + \underbrace{\omega_0}_{2} \underbrace{(L-\mathcal{R})^3}_{3}$$

$$= (L-\mathcal{R}) \left(-\underbrace{\omega_0 \mathcal{R}}_{3} + \omega_0 \mathcal{R} - \underbrace{\omega_0}_{2} \frac{\mathcal{R}^2}{3} + \underbrace{\omega_0}_{3} (\underbrace{V^2 - 2L\mathcal{R} + \mathcal{R}^2}_{2})\right)$$

$$= (L-\mathcal{R}) \left(\underbrace{\omega_0 \mathcal{R}}_{3} - \underbrace{\omega_0 \mathcal{R}^2}_{6L}\right) \implies M_{\mathcal{R}} = \underbrace{\omega_0 L}_{2} \mathcal{R} - \underbrace{\omega_0 \mathcal{R}^2}_{2} + \underbrace{\omega_0 \mathcal{R}^3}_{6L}$$

