Response of SDOF System to Harmonic Loading

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- External energy supplied to system as applied force or imposed motion (displacement, velocity or acceleration)
- This section deals only with *harmonic excitation* which results in *harmonic response*
- Harmonic forcing function takes the form:

 $F(t) = F_0 e^{i(\omega t + \phi)} \quad or \quad F(t) = F_0 \cos(\omega t + \phi) \quad or \quad F(t) = F_0 \sin(\omega t + \phi)$

- Where F_0 is the amplitude, ω the frequency and ϕ the phase angle.
- The response of a linear system subjected to harmonic excitation is also harmonic.
- The response amplitude depends on the ratio of the excitation frequency to the natural frequency.
- Some "common" harmonic forcing functions are:
 - Rotating machine / element with (large) residual imbalance
 - Vehicle travelling on pavement corrugations or sinusoidal surfaces

Response of SDOF System to Harmonic Loading

• Equation of motion when a force is applied to a viscously damped SDOF system is:

 $m\ddot{x} + c\dot{x} + kx = F(t) \quad \leftarrow \text{ non homogeneous differential eqn.}$

- The general solution to a nonhomogeneous DE is the sum if the homogeneous solution $x_h(t)$ and the particular solution $x_p(t)$.
- The homogeneous solution represents the solution to the free SDOF which is known to decay over time for all conditions (underdamped, critically damped and overdamped).
- The general solution therefore reduces to the particular solution $x_p(t)$ which represents the steady-state vibration which exists as long as the forcing function is applied.

Response of SDOF System to Harmonic Loading

• Example of solution to harmonically excited damped SDOF system:



• Let the forcing function acting on the mass of an undamped SDOF system be:

$$F(t) = F_0 \cos(\omega t)$$

• The eqn. of motion reduces to:

$$m\ddot{x} + kx = F_0 \cos(\omega t)$$

• Where the homogeneous solution is:

$$x_h(t) = C_1 \cos(\omega_n t) + C_2 \sin(\omega_n t)$$

where $\omega_n = \sqrt{k/m}$

• As the excitation is harmonic, the particular solution is also harmonic with the same frequency:

$$x_p(t) = X \cos(\omega t)$$

• Substituting $x_p(t)$ in the eqn. of motion and solving for X gives:

$$X = \frac{F_0}{k - m\omega^2}$$

• The complete solution becomes

$$x(t) = x_h(t) + x_p(t) = C_1 \cos(\omega_n t) + C_2 \sin(\omega_n t) + \frac{F_0}{k - m\omega^2} \cos(\omega t)$$

• Applying the initial conditions $x(t=0) = x_0$ and $\dot{x}(t=0) = \dot{x}_0$ gives:

$$C_1 = x_0 - \frac{F_0}{k - m\omega^2}$$
 and $C_2 = \frac{\dot{x}_0}{\omega_n}$

• The complete solution becomes:

$$x(t) = \left(x_0 - \frac{F_0}{k - m\omega^2}\right) \cos(\omega_n t) + \left(\frac{\dot{x}_0}{\omega_n}\right) \sin(\omega_n t) + \frac{F_0}{k - m\omega^2} \cos(\omega t)$$

• The maximum amplitude of the steady-state solution can be written as:

$$\frac{X}{\delta_{st}} = \frac{1}{1 - \left(\frac{\omega}{\omega_n}\right)^2} \qquad \text{where } \delta_{st} = \frac{F_0}{k}$$

• X/δ_{st} is the ratio of the dynamic to the static amplitude and is known as the **amplification factor** or **amplification ratio** and is dependent on the frequency ratio $r = \omega/\omega_n$.

- When $\omega/\omega_n < 1$ the denominator of the steady-state amplitude is positive and the amplification factor increases as ω approaches the natural frequency ω_n . The response is *in-phase* with the excitation.
- When $\omega/\omega_n > 1$ the denominator of the steady-state amplitude is negative an the amplification factor is redefined as:

$$\frac{X}{\delta_{st}} = \frac{1}{\left(\frac{\omega}{\omega_n}\right)^2 - 1}$$

and the steady – state response becomes :

$$x_p(t) = -X \cos(\omega t)$$

which shows that the response is out-of-phase with the excitation and decreases (\rightarrow zero) as ω increases ($\rightarrow \infty$)



• When $\omega/\omega_n = 1$ the denominator of the steady-state amplitude is zero an the response becomes infinitely large. This condition when $\omega = \omega_n$ is known as resonance.



• The complete solution

$$x(t) = \left(x_0 - \frac{F_0}{k - m\omega^2}\right) \cos(\omega_n t) + \left(\frac{\dot{x}_0}{\omega_n}\right) \sin(\omega_n t) + \frac{F_0}{k - m\omega^2} \cos(\omega t)$$

can be written as:

$$\begin{aligned} x(t) &= A\cos(\omega_n t + \phi) + \frac{\delta_{st}}{1 - \left(\frac{\omega}{\omega_n}\right)^2} \cos(\omega t) & \text{for } \omega / \omega_n < 1 \\ x(t) &= A\cos(\omega_n t + \phi) - \frac{\delta_{st}}{1 - \left(\frac{\omega}{\omega_n}\right)^2} \cos(\omega t) & \text{for } \omega / \omega_n > 1 \end{aligned}$$

where A and ϕ are functions of x_0 and \dot{x}_0 as before.

• The complete solution is a sum of two cosines with frequencies corresponding to the natural and forcing (excitation) frequencies.

Steady-state Solution

• If the forcing function is harmonic:

$$F(t) = F_0 \cos(\omega t)$$

• The equation of motion of a SDOF system with viscous damping is:

 $m\ddot{x} + c\dot{x} + kx = F_0 \cos(\omega t)$

• The steady-state response is given by the particular solution which is also expected to be harmonic:

 $x_p(t) = X \cos(\omega t - \phi)$

where the amplitude X and the phase angle ϕ are to be determined

• Substituting x_p into the steady-state eqn. of motion yields:

$$X\left[\left(k-m\omega^{2}\right)\cos(\omega t-\phi)-\cos(\omega t-\phi)\right]=F_{0}\cos(\omega t)$$

applying the trigonometric relationships :

$$cos(\omega t - \phi) = cos(\omega t) cos(\phi) + sin(\omega t) sin(\phi)$$

$$sin(\omega t - \phi) = sin(\omega t) cos(\phi) - cos(\omega t) sin(\phi)$$

we obtain :

$$X\left[\left(k - m\omega^{2}\right)\cos(\phi) + c\omega\sin(\phi)\right] = F_{0}$$
$$X\left[\left(k - m\omega^{2}\right)\sin(\phi) - c\omega\cos(\phi)\right] = 0$$

which gives :

$$X = \frac{F_0}{\left[\left(k - m\omega^2\right)^2 + (c\omega)^2\right]^{1/2}} \quad and \quad \phi = tan^{-1}\left(\frac{c\omega}{k - m\omega^2}\right)$$

for the particular solution

$$x_p(t) = X \cos(\omega t - \phi)$$

• Alternatively, the amplitude and phase can be written in terms of the frequency ratio $r = \omega/\omega_n$ and the damping coefficient ζ :

$$\frac{X}{\delta_{st}} = \frac{1}{\left\{ \left[1 - \left(\frac{\omega}{\omega_n}\right)^2 \right]^2 + \left[2\zeta \frac{\omega}{\omega_n} \right]^2 \right\}^{\frac{1}{2}}} = \frac{1}{\left\{ \left[1 - r^2 \right]^2 + \left[2\zeta r \right]^2 \right\}^{\frac{1}{2}}}$$

$$\phi = a \tan \left(\frac{2\zeta \frac{\omega}{\omega_n}}{1 - \left(\frac{\omega}{\omega_n}\right)^2} \right) = a \tan \left(\frac{2\zeta r}{1 - r^2} \right)$$

$$\frac{X}{\delta_{st}} = \frac{1}{\left\{ \left[1 - r^2 \right]^2 + \left[2\zeta r \right]^2 \right\}^{1/2}} \qquad \phi = a \tan\left(\frac{2\zeta r}{1 - r^2}\right)$$





- The magnification ratio at all frequencies is reduced with increased damping.
- The effect of damping on the magnification ratio is greatest at or near resonance.
- The magnification ratio approaches 1 as the frequency ratio approaches 0.
- The magnification ratio approaches 0 as the frequency ratio approaches ∞



- For undamped systems ($\zeta = 0$) the phase angle is 0° (response in phase with excitation) for r<1 and 180° (response out of phase with excitation) for r>1.
- For damped systems ($\zeta > 0$) when r < 1 the phase angle is less than 90° and response lags the excitation and when r > 1 the phase angle is greater than 90° and the response leads the excitation (approaches 180° for large frequency ratios..
- For damped systems ($\zeta > 0$) when r = 1 the phase lag is always 90°.



Complete Solution

• The complete solution is the sum of the homogeneous solution $x_h(t)$ and the particular solution $x_p(t)$:

$$x(t) = X_0 e^{-\zeta \omega_n t} \cos(\omega_d t - \phi_0) + X \cos(\omega t - \phi)$$

where $\omega_d = \omega_n \sqrt{1 - \zeta^2}$, X and ϕ are given as before, and X_0 and ϕ_0 are determined from the initial conditions