



2D Truss Analysis Using Stiffness Method

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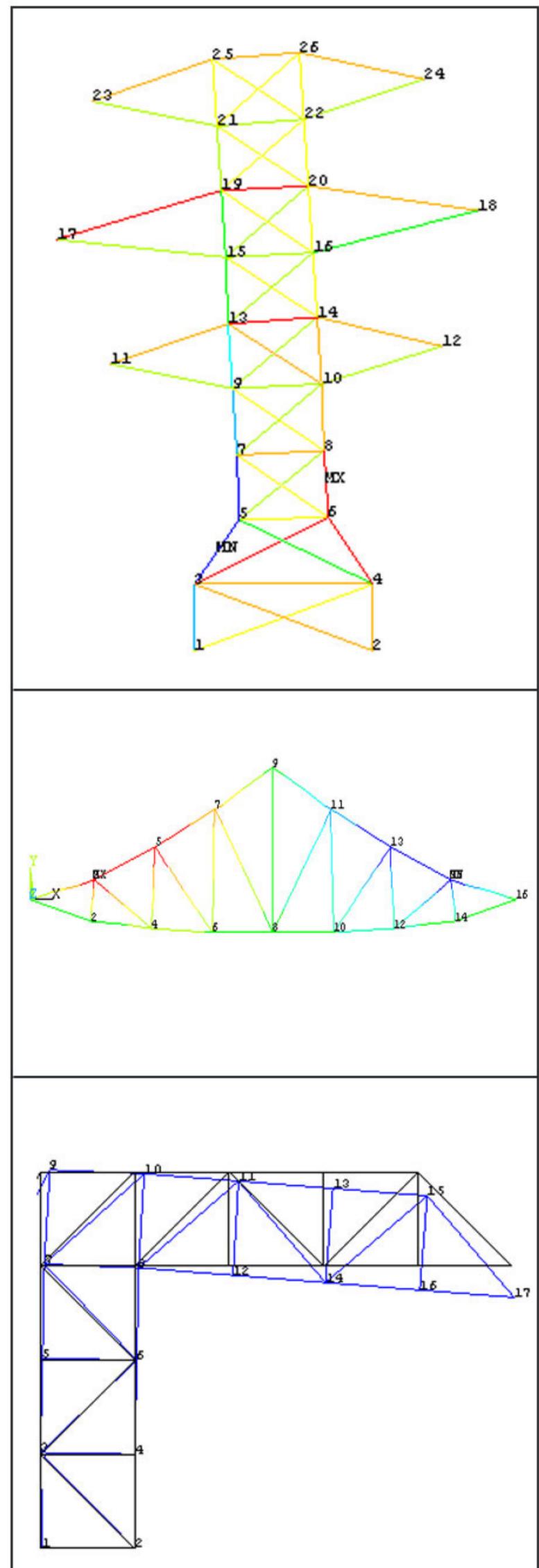
Special thanks to Prof. Eysa Salajegheh, Civil Eng. Dept., University of Kerman, Kerman, Iran.



2D Truss Analysis Using Stiffness Method

This program is able to analyze all types of 2-D trusses (with all degree of freedom) using stiffness method (matrix analysis) under any kind of concentrated nodal loadings (F_x , F_y) and submit values of supportive reactions, nodal displacements, axial forces and element stresses and strains as MATLAB output. General feature of this program includes one "m-file" and an "Excel" input file which to run this program both of them (truss.m and Truss.xls) must be saved in MATLAB directory. Meanwhile notice that input file (Truss.xls) must be saved as "Excel 2003". Using this program is very easy and user friendly (i.e. for each new example adjust input file and then save it. In entering file, some questions are asked and some tables exist which are related to problem inputs. In this file, variables are shown in blue color). Then using MATLAB software run "truss.m" file, later you can see results in MATLAB's command window.

Finally, to test this program, different Examples are given which in these examples program outputs are compared with the results from ABAQUS or ANSYS software. Similarity of results shows that this program works without any deficiencies as well as these two softwares.





```

=====
%      2D truss analysis using stiffness method (matrix analysis)
%      Written by: "Sobhan Rostami & Ali Moeinadini"
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=====

clc
clear all

%Input data:
NN=xlsread('Truss','input','E8');
Coor=xlsread('Truss','input','C14:E250');
for j=1:NN
    i=Coor(j,1);
    X(i)=Coor(j,2);
    Y(i)=Coor(j,3);
end

NE=xlsread('Truss','input','E9');
Pro=xlsread('Truss','input','N11:R250');
for j=1:NE
    i=Pro(j,1);
    E(i)=Pro(j,2);
    A(i)=Pro(j,3);
    Dir(i,1)=i;
    Dir(i,2)=Pro(j,4);
    Dir(i,3)=Pro(j,5);
end

NC=xlsread('Truss','input','AD8');
Cons=xlsread('Truss','input','Y14:Z26');

NF=xlsread('Truss','input','AB27');
Forc=xlsread('Truss','input','Y30:AA250');

%Definition of Global stiffness submatrixes for each element:
for i=1:NE
    L(i)=sqrt((X(Dir(i,3))-X(Dir(i,2)))^2+(Y(Dir(i,3))-Y(Dir(i,2)))^2);
    cos(i)=(X(Dir(i,3))-X(Dir(i,2)))/L(i);
    sin(i)=(Y(Dir(i,3))-Y(Dir(i,2)))/L(i);
end

for i=1:NE
    S(i)=E(i)*A(i)/L(i);
    k11(:, :, i)=S(i)*[(cos(i))^2 sin(i)*cos(i);sin(i)*cos(i) (sin(i))^2];
    k12(:, :, i)=-k11(:, :, i);
    k21(:, :, i)=k12(:, :, i);
    k22(:, :, i)=k11(:, :, i);
end

%Definition of structure stiffness matrix(plant of submatrixes):
K=zeros(2*NN,2*NN);
for n=1:NE
    i=Dir(n,2);
    j=Dir(n,3);
    K(2*i-1:2*i,2*i-1:2*i)=k11(:, :, n)+ K(2*i-1:2*i,2*i-1:2*i);
    K(2*i-1:2*i,2*j-1:2*j)=k12(:, :, n);
    K(2*j-1:2*j,2*i-1:2*i)=k21(:, :, n);
    K(2*j-1:2*j,2*j-1:2*j)=k22(:, :, n)+ K(2*j-1:2*j,2*j-1:2*j);
End

%Definition of primary external nodal forces vector:
F=zeros(2*NN,1);
for i=1:NF
    r=2*Forc(i,1);
    F(r-1)=Forc(i,2);
    F(r)=Forc(i,3);
end

```



```
%Elimination of rows and columns of K-matrix concern to supports:
```

```
S=K;
for i=1:NC
    r=2*Cons(i,1);
    if Cons(i,2)==0
        S(r-1,:)=0; S(:,r-1)=0; S(r-1,r-1)=1;
        S(r,:)=0; S(:,r)=0; S(r,r)=1;
    elseif Cons(i,2)==1
        S(r-1,:)=0; S(:,r-1)=0; S(r-1,r-1)=1;
    else
        S(r,:)=0; S(:,r)=0; S(r,r)=1;
    end
end
end
```

```
%-----%
```

```
%Solution of equation "{F}=[S]{d}" by Gauss elimination method:
```

```
n=2*NN;
```

```
%creation of upper triangular matrix
```

```
s=0;
for j=1:n-1
    if S(j,j)==0
        k=j;
        for k=k+1:n
            if S(k,j)==0
                continue
            end
            break
        end
        B=S(j,:); C=F(j);
        S(j,:)=S(k,:); F(j)=F(k);
        S(k,:)=B; F(k)=C;
    end
    for i=1+s:n-1
        L=S(i+1,j)/S(j,j);
        S(i+1,:)=S(i+1,:)-L*S(j,:);
        F(i+1)=F(i+1)-L*F(j);
    end
    s=s+1;
end
```

```
%solution of equations
```

```
d=zeros(2*NN,1);
d(n)=F(n)/S(n,n);
for i=n-1:-1:1
    sum=0;
    for j=i+1:n
        sum=sum+S(i,j)*d(j);
    end
    d(i)=(1/S(i,i))*(F(i)-sum);
end
```

```
%-----%
```

```
%Creation of external nodal forces vector:
```

```
W=K*d;
```

```
%Calculation of elements axial force:
```

```
for n=1:NE
    i=Dir(n,2);
    j=Dir(n,3);
    PJ=k21(:, :, n)*[d(2*i-1);d(2*i)]+ k22(:, :, n)*[d(2*j-1);d(2*j)];
    P(n)=PJ(1)*cos(n)+PJ(2)*sin(n);
    stress(n)=P(n)/A(n);
    strain(n)=stress(n)/E(n);
end
```



```

%Analysis results:
disp('2D-truss Analysis (OUTPUTS)')
disp('*****')
disp(' ')
disp('Node displacement :')
disp(' ')
for i=1:NN
    fprintf('dx%g\t',i); fprintf('= %G\n',d(2*i-1))
    fprintf('dy%g\t',i); fprintf('= %G\n',d(2*i))
    disp(' ')
end
disp('~~~~~')

disp('Support reactions :')
disp(' ')
for i=1:NC
    r=2*Cons(i,1);
    if Cons(i,2)==0
        fprintf('Rx%g\t',r/2); fprintf('= %G\n',W(r-1))
        fprintf('RY%g\t',r/2); fprintf('= %G\n',W(r))
    elseif Cons(i,2)==1
        fprintf('Rx%g\t',r/2); fprintf('= %G\n',W(r-1))
    else
        fprintf('Ry%g\t',r/2); fprintf('= %G\n',W(r))
    end
end
disp('~~~~~')

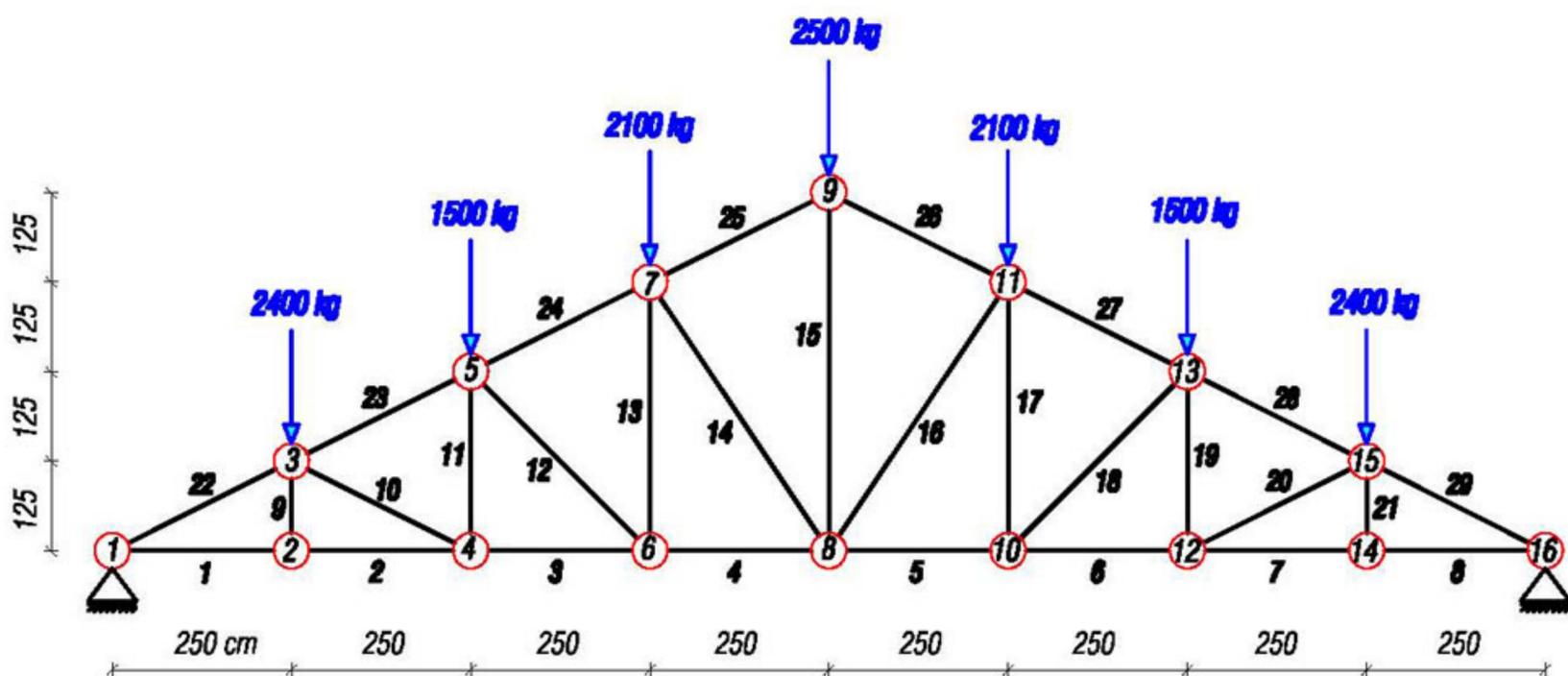
disp('Elements force :')
disp(' ')
for i=1:NE
    fprintf('P%g\t',i); fprintf('= %G\n',P(i))
end
disp('~~~~~')

disp('Elements stress :')
disp(' ')
for i=1:NE
    fprintf('Stress%g\t',i); fprintf('= %G\n',stress(i))
end
disp('~~~~~')

disp('Elements strain :')
disp(' ')
for i=1:NE
    fprintf('Strain%g\t',i); fprintf('= %G\n',strain(i))
end
disp('~~~~~')
disp('Finished!')
disp('Thank you for using of this Program')

```

Example 1 : Determine the reactions, nodal displacements, elements forces, elements stresses and strains for 2-D truss which is given then check the results with ANSYS software. (force unit is Kg and distance unit is Cm)



Modulus of Elasticity (E) : $2.1E+6 \text{ kg/cm}^2$

The area cross section for element number '15' is 20cm^2 and for the others is 15cm^2 .



| Node displacement : | | Elements force : | | Elements stress : | | Elements strain : | |
|---------------------|----------------|------------------|------------|-------------------|------------|-------------------|----------------|
| dx1 | = 0 | P1 | = 1650 | Stress1 | = 110 | Strain1 | = 5.23810E-05 |
| dy1 | = 0 | P2 | = 1650 | Stress2 | = 110 | Strain2 | = 5.23810E-05 |
| dx2 | = 0.0130952 | P3 | = -750 | Stress3 | = -50 | Strain3 | = -2.38095E-05 |
| dy2 | = -0.695788 | P4 | = -2550 | Stress4 | = -170 | Strain4 | = -8.09524E-05 |
| dx3 | = 0.187066 | P5 | = -2550 | Stress5 | = -170 | Strain5 | = -8.09524E-05 |
| dy3 | = -0.695788 | P6 | = -750 | Stress6 | = -50 | Strain6 | = -2.38095E-05 |
| dx4 | = 0.0261905 | P7 | = 1650 | Stress7 | = 110 | Strain7 | = 5.23810E-05 |
| dy4 | = -0.964299 | P8 | = 1650 | Stress8 | = 110 | Strain8 | = 5.23810E-05 |
| dx5 | = 0.182351 | P9 | = 0 | Stress9 | = 0 | Strain9 | = 0.00000E+00 |
| dy5 | = -0.954775 | P10 | = -2683.28 | Stress10 | = -178.885 | Strain10 | = -8.51835E-05 |
| dx6 | = 0.0202381 | P11 | = 1200 | Stress11 | = 80 | Strain11 | = 3.80952E-05 |
| dy6 | = -1.07648 | P12 | = -2545.58 | Stress12 | = -169.706 | Strain12 | = -8.08122E-05 |
| dx7 | = 0.118246 | P13 | = 1800 | Stress13 | = 120 | Strain13 | = 5.71429E-05 |
| dy7 | = -1.05505 | P14 | = -3515.41 | Stress14 | = -234.361 | Strain14 | = -1.11600E-04 |
| dx8 | = -3.50577E-16 | P15 | = 5850 | Stress15 | = 292.5 | Strain15 | = 1.39286E-04 |
| dy8 | = -1.07343 | P16 | = -3515.41 | Stress16 | = -234.361 | Strain16 | = -1.11600E-04 |
| dx9 | = 3.793E-16 | P17 | = 1800 | Stress17 | = 120 | Strain17 | = 5.71429E-05 |
| dy9 | = -1.00379 | P18 | = -2545.58 | Stress18 | = -169.706 | Strain18 | = -8.08122E-05 |
| dx10 | = -0.0202381 | P19 | = 1200 | Stress19 | = 80 | Strain19 | = 3.80952E-05 |
| dy10 | = -1.07648 | P20 | = -2683.28 | Stress20 | = -178.885 | Strain20 | = -8.51835E-05 |
| dx11 | = -0.118246 | P21 | = 0 | Stress21 | = 0 | Strain21 | = 0.00000E+00 |
| dy11 | = -1.05505 | P22 | = -16211.5 | Stress22 | = -1080.77 | Strain22 | = -5.14651E-04 |
| dx12 | = -0.0261905 | P23 | = -13528.2 | Stress23 | = -901.881 | Strain23 | = -4.29467E-04 |
| dy12 | = -0.964299 | P24 | = -11515.8 | Stress24 | = -767.717 | Strain24 | = -3.65579E-04 |
| dx13 | = -0.182351 | P25 | = -9335.58 | Stress25 | = -622.372 | Strain25 | = -2.96368E-04 |
| dy13 | = -0.954775 | P26 | = -9335.58 | Stress26 | = -622.372 | Strain26 | = -2.96368E-04 |
| dx14 | = -0.0130952 | P27 | = -11515.8 | Stress27 | = -767.717 | Strain27 | = -3.65579E-04 |
| dy14 | = -0.695788 | P28 | = -13528.2 | Stress28 | = -901.881 | Strain28 | = -4.29467E-04 |
| dx15 | = -0.187066 | P29 | = -16211.5 | Stress29 | = -1080.77 | Strain29 | = -5.14651E-04 |
| dy15 | = -0.695788 | | | | | | |
| dx16 | = 0 | | | | | | |
| dy16 | = 0 | | | | | | |



PRINT U NODAL SOLUTION PER NODE

***** POST1 NODAL DEGREE OF FREEDOM LISTING *****

LOAD STEP= 1 SUBSTEP= 1
TIME= 1.0000 LOAD CASE= 0

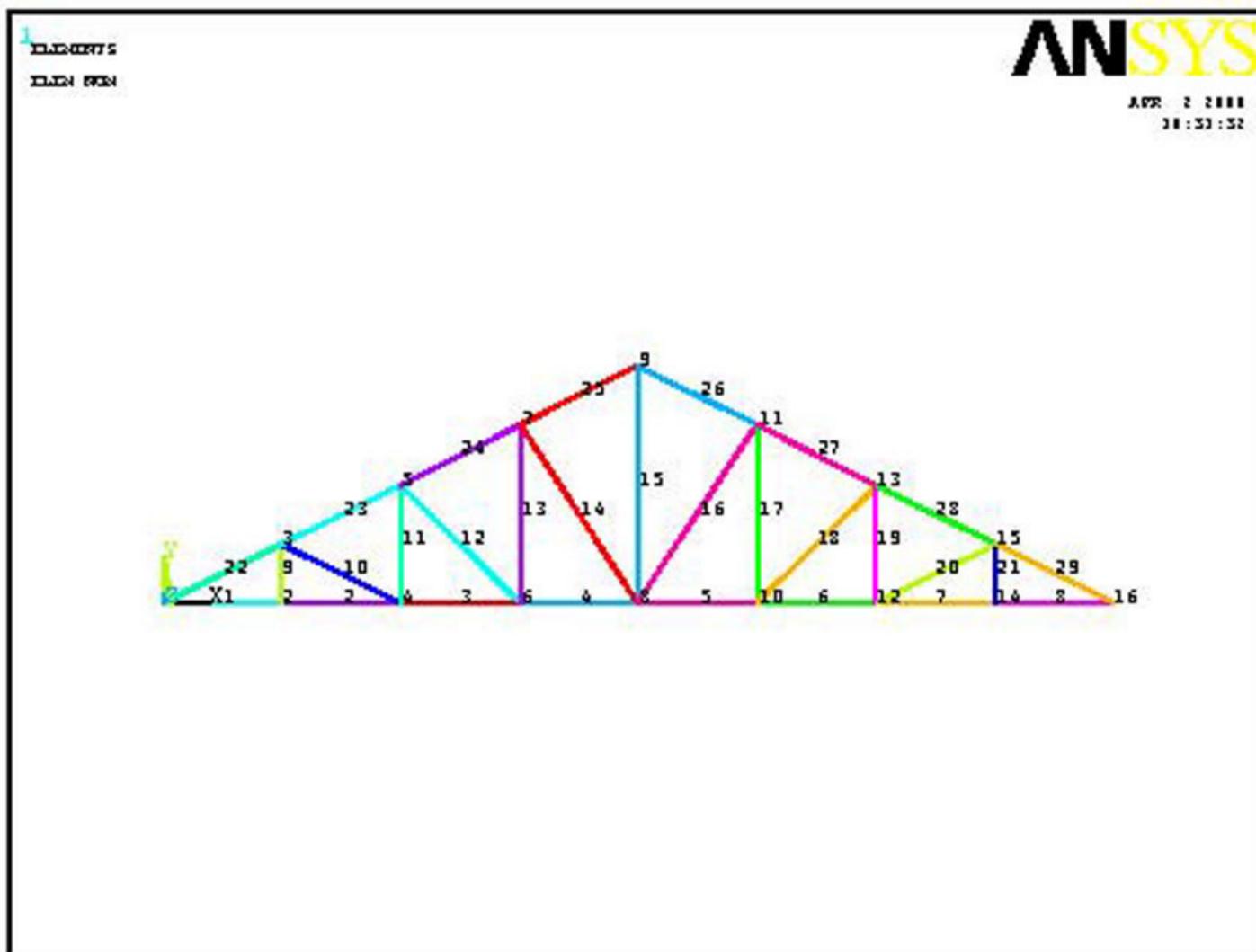
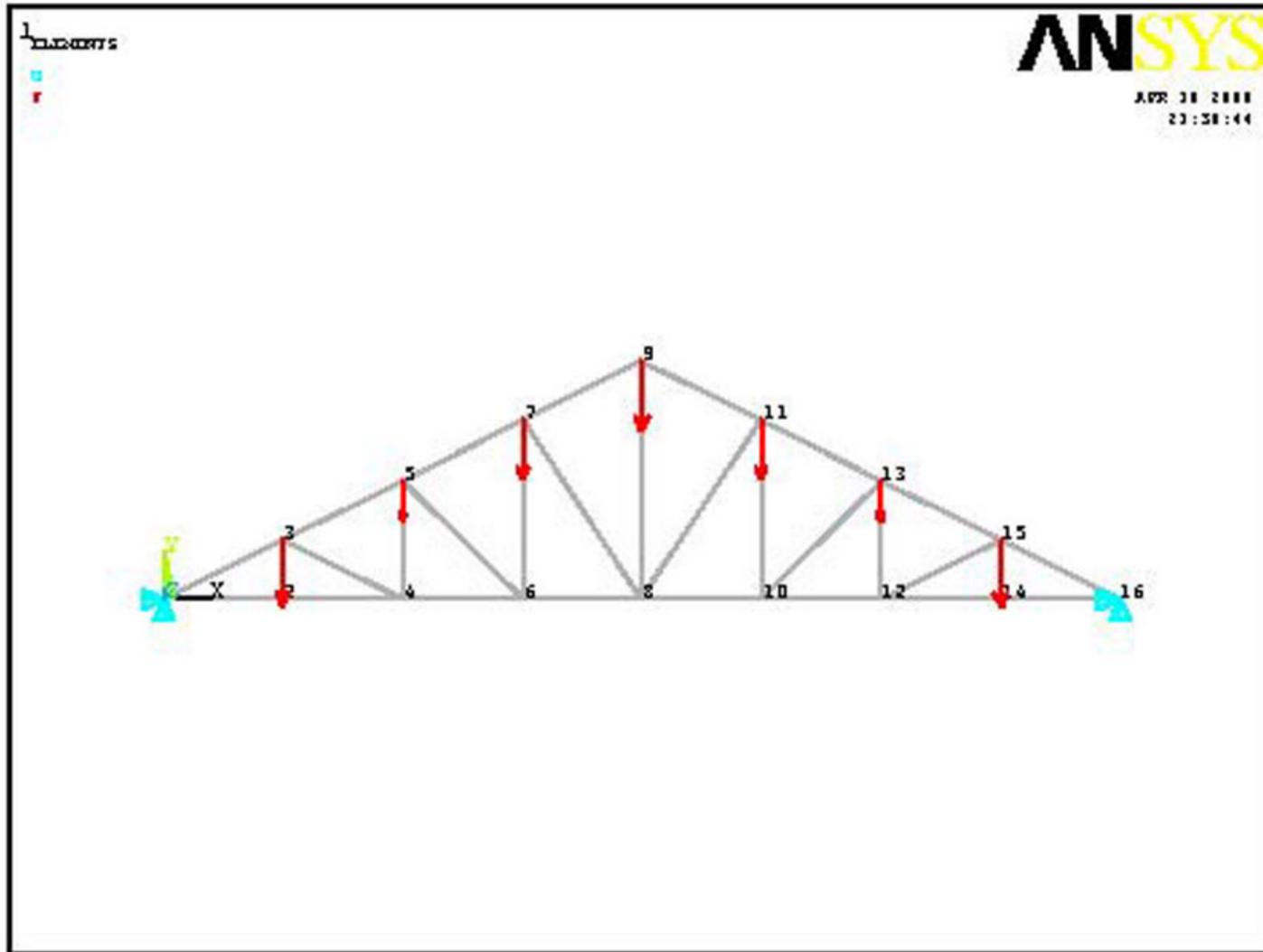
THE FOLLOWING DEGREE OF FREEDOM RESULTS ARE IN THE GLOBAL COORDINATE SYSTEM

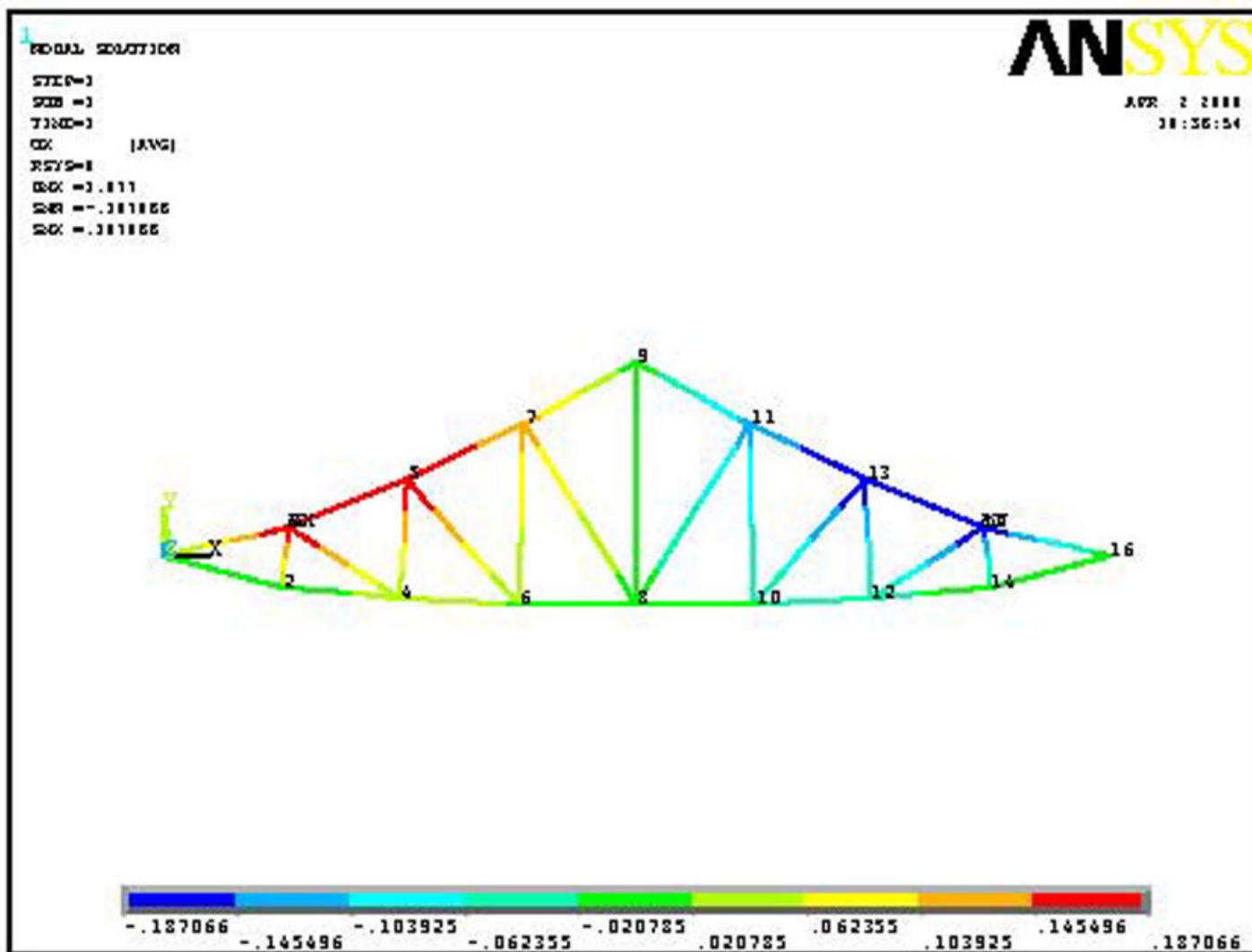
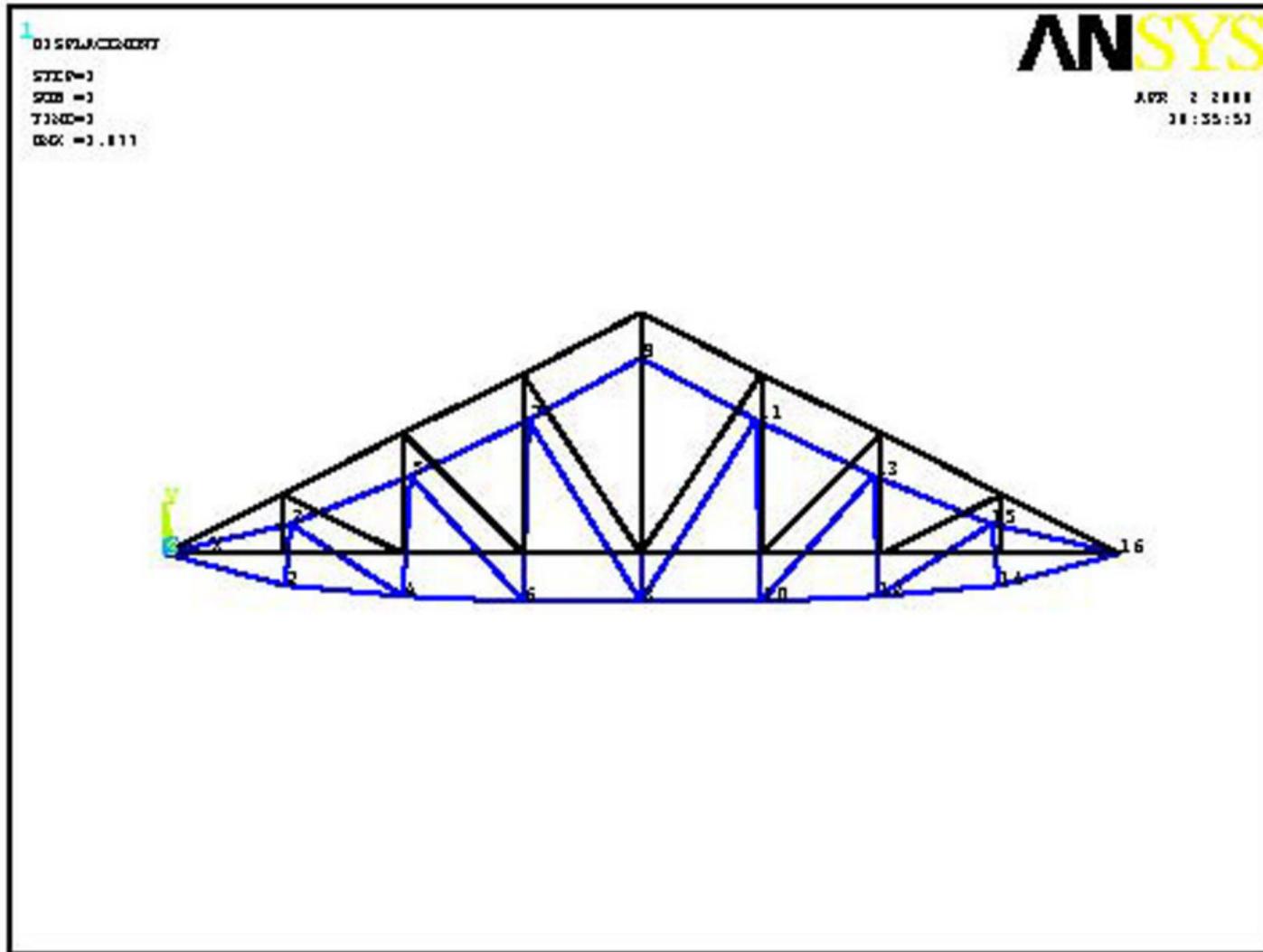
| NODE | UX | UY | UZ | USUM |
|------|--------------|----------|--------|---------|
| 1 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 2 | 0.13095E-01 | -0.69579 | 0.0000 | 0.69591 |
| 3 | 0.18707 | -0.69579 | 0.0000 | 0.72050 |
| 4 | 0.26190E-01 | -0.96430 | 0.0000 | 0.96465 |
| 5 | 0.18235 | -0.95477 | 0.0000 | 0.97203 |
| 6 | 0.20238E-01 | -1.0765 | 0.0000 | 1.0767 |
| 7 | 0.11825 | -1.0551 | 0.0000 | 1.0617 |
| 8 | -0.91990E-16 | -1.0734 | 0.0000 | 1.0734 |
| 9 | 0.21756E-16 | -1.0038 | 0.0000 | 1.0038 |
| 10 | -0.20238E-01 | -1.0765 | 0.0000 | 1.0767 |
| 11 | -0.11825 | -1.0551 | 0.0000 | 1.0617 |
| 12 | -0.26190E-01 | -0.96430 | 0.0000 | 0.96465 |
| 13 | -0.18235 | -0.95477 | 0.0000 | 0.97203 |
| 14 | -0.13095E-01 | -0.69579 | 0.0000 | 0.69591 |
| 15 | -0.18707 | -0.69579 | 0.0000 | 0.72050 |
| 16 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

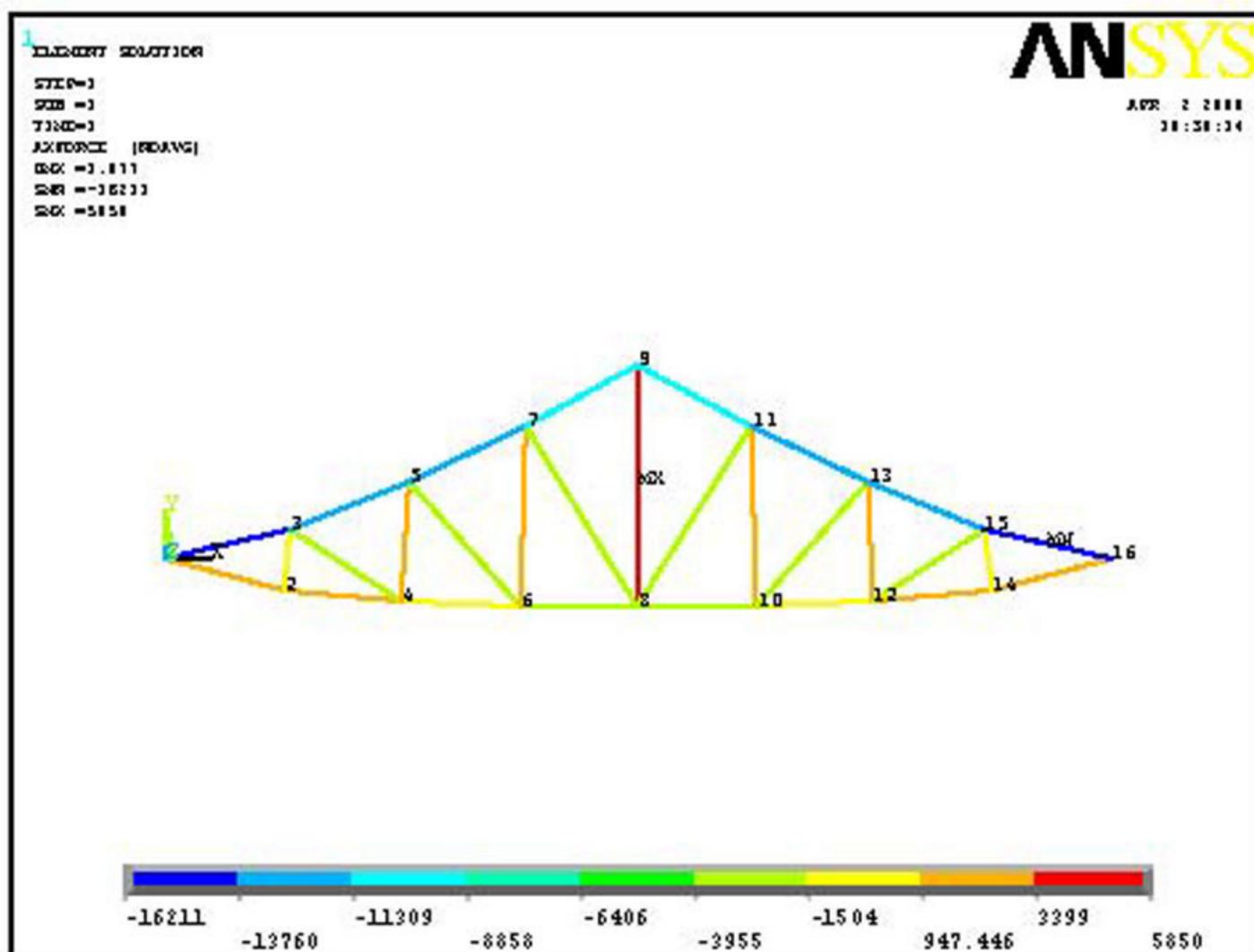
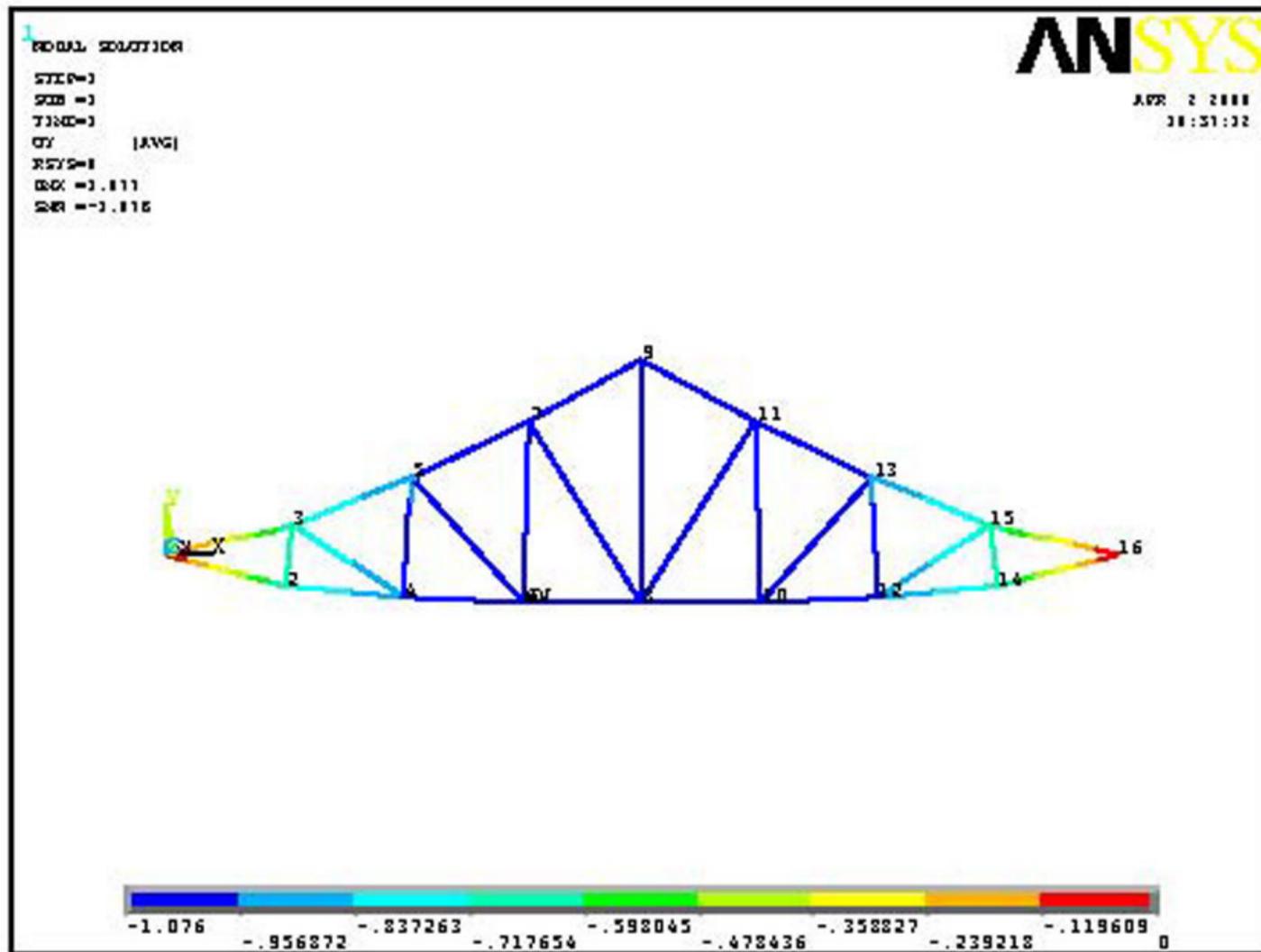
PRINT ELEMENT TABLE ITEMS PER ELEMENT

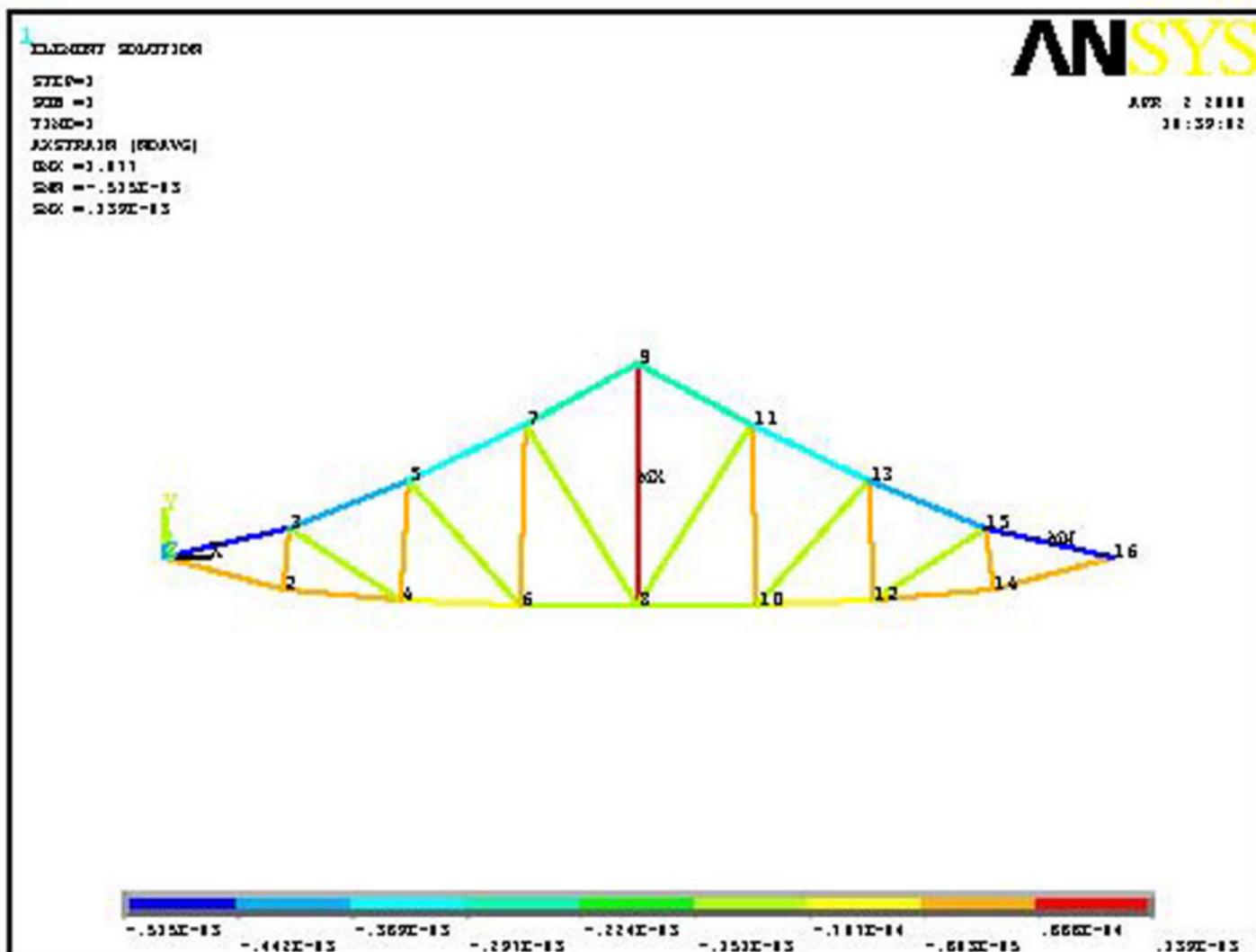
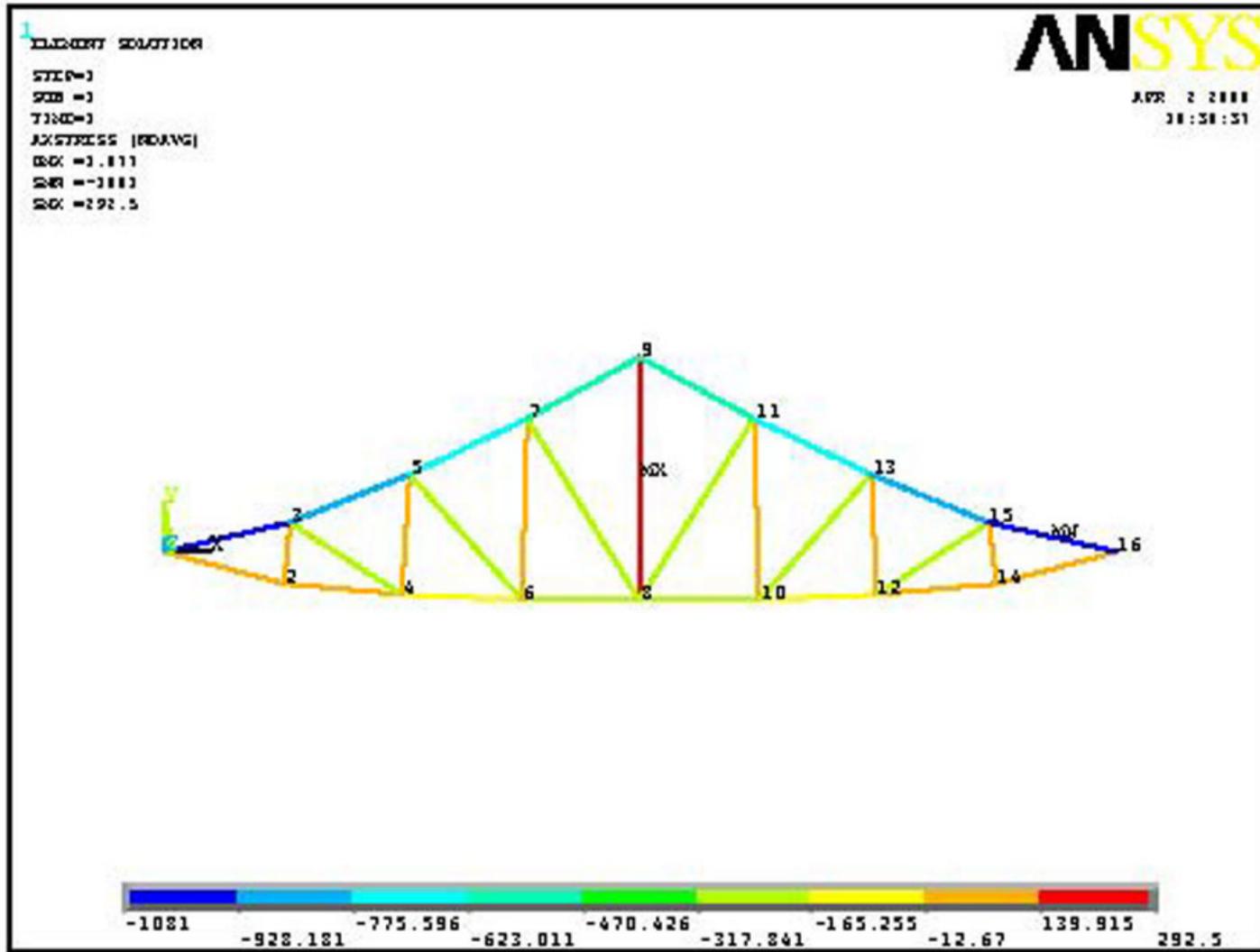
***** POST1 ELEMENT TABLE LISTING *****

| STAT | CURRENT | CURRENT | CURRENT |
|------|---------|----------|--------------|
| ELEM | AXFORCE | AXSTRESS | AXSTRAIN |
| 1 | 1650.0 | 110.00 | 0.52381E-04 |
| 2 | 1650.0 | 110.00 | 0.52381E-04 |
| 3 | -750.00 | -50.000 | -0.23810E-04 |
| 4 | -2550.0 | -170.00 | -0.80952E-04 |
| 5 | -2550.0 | -170.00 | -0.80952E-04 |
| 6 | -750.00 | -50.000 | -0.23810E-04 |
| 7 | 1650.0 | 110.00 | 0.52381E-04 |
| 8 | 1650.0 | 110.00 | 0.52381E-04 |
| 9 | 0.0000 | 0.0000 | 0.0000 |
| 10 | -2683.3 | -178.89 | -0.85184E-04 |
| 11 | 1200.0 | 80.000 | 0.38095E-04 |
| 12 | -2545.6 | -169.71 | -0.80812E-04 |
| 13 | 1800.0 | 120.00 | 0.57143E-04 |
| 14 | -3515.4 | -234.36 | -0.11160E-03 |
| 15 | 5850.0 | 292.50 | 0.13929E-03 |
| 16 | -3515.4 | -234.36 | -0.11160E-03 |
| 17 | 1800.0 | 120.00 | 0.57143E-04 |
| 18 | -2545.6 | -169.71 | -0.80812E-04 |
| 19 | 1200.0 | 80.000 | 0.38095E-04 |
| 20 | -2683.3 | -178.89 | -0.85184E-04 |
| 21 | 0.0000 | 0.0000 | 0.0000 |
| 22 | -16211. | -1080.8 | -0.51465E-03 |
| 23 | -13528. | -901.88 | -0.42947E-03 |
| 24 | -11516. | -767.72 | -0.36558E-03 |
| 25 | -9335.6 | -622.37 | -0.29637E-03 |
| 26 | -9335.6 | -622.37 | -0.29637E-03 |
| 27 | -11516. | -767.72 | -0.36558E-03 |
| 28 | -13528. | -901.88 | -0.42947E-03 |
| 29 | -16211. | -1080.8 | -0.51465E-03 |

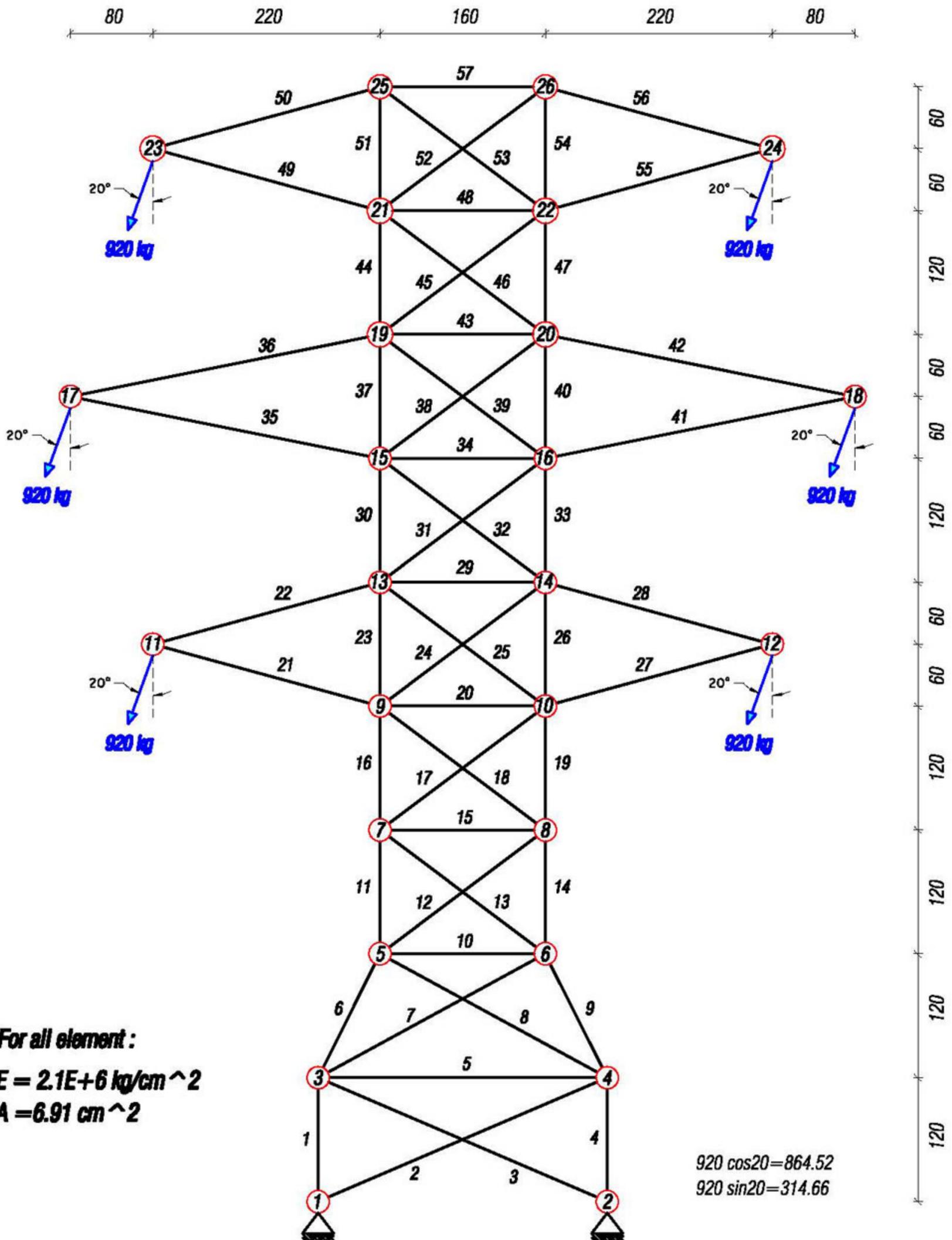








Example 2: Determine the reactions, nodal displacements, elements forces, elements stresses and strains for 2-D truss which is given then check the results with ANSYS software. (force unit is Kg and distance unit is Cm)





2D truss analysis using stiffness method (matrix analysis)

Page2/3

Written by : " Sobhan Rostami & Ali Moeinadini "

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" Input Data in Excel "

% Please insert properties of the elements, respect to elements ID :

| ID | E | A | Start | End |
|----|----------|------|-------|-----|
| 1 | 2.10E+06 | 6.91 | 1 | 3 |
| 2 | 2.10E+06 | 6.91 | 1 | 4 |
| 3 | 2.10E+06 | 6.91 | 2 | 3 |
| 4 | 2.10E+06 | 6.91 | 2 | 4 |
| 5 | 2.10E+06 | 6.91 | 3 | 4 |
| 6 | 2.10E+06 | 6.91 | 3 | 5 |
| 7 | 2.10E+06 | 6.91 | 3 | 6 |
| 8 | 2.10E+06 | 6.91 | 4 | 5 |
| 9 | 2.10E+06 | 6.91 | 4 | 6 |
| 10 | 2.10E+06 | 6.91 | 5 | 6 |
| 11 | 2.10E+06 | 6.91 | 5 | 7 |
| 12 | 2.10E+06 | 6.91 | 5 | 8 |
| 13 | 2.10E+06 | 6.91 | 6 | 7 |
| 14 | 2.10E+06 | 6.91 | 6 | 8 |
| 15 | 2.10E+06 | 6.91 | 7 | 8 |
| 16 | 2.10E+06 | 6.91 | 7 | 9 |
| 17 | 2.10E+06 | 6.91 | 7 | 10 |
| 18 | 2.10E+06 | 6.91 | 8 | 9 |
| 19 | 2.10E+06 | 6.91 | 8 | 10 |
| 20 | 2.10E+06 | 6.91 | 9 | 10 |
| 21 | 2.10E+06 | 6.91 | 9 | 11 |
| 22 | 2.10E+06 | 6.91 | 11 | 13 |
| 23 | 2.10E+06 | 6.91 | 9 | 13 |
| 24 | 2.10E+06 | 6.91 | 9 | 14 |
| 25 | 2.10E+06 | 6.91 | 10 | 13 |
| 26 | 2.10E+06 | 6.91 | 10 | 14 |
| 27 | 2.10E+06 | 6.91 | 10 | 12 |
| 28 | 2.10E+06 | 6.91 | 12 | 14 |
| 29 | 2.10E+06 | 6.91 | 13 | 14 |
| 30 | 2.10E+06 | 6.91 | 13 | 15 |
| 31 | 2.10E+06 | 6.91 | 13 | 16 |
| 32 | 2.10E+06 | 6.91 | 14 | 15 |
| 33 | 2.10E+06 | 6.91 | 14 | 16 |
| 34 | 2.10E+06 | 6.91 | 15 | 16 |
| 35 | 2.10E+06 | 6.91 | 15 | 17 |
| 36 | 2.10E+06 | 6.91 | 17 | 19 |
| 37 | 2.10E+06 | 6.91 | 15 | 19 |
| 38 | 2.10E+06 | 6.91 | 15 | 20 |
| 39 | 2.10E+06 | 6.91 | 16 | 19 |
| 40 | 2.10E+06 | 6.91 | 16 | 20 |
| 41 | 2.10E+06 | 6.91 | 16 | 18 |
| 42 | 2.10E+06 | 6.91 | 18 | 20 |

E : Modulus of elasticity

A : Area cross section

Start : start node of element

End : end node of element



| Node displacement : | | Elements force : | | Elements stress : | | Elements strain : | |
|---------------------|--------------|------------------|------------|-------------------|------------|-------------------|----------------|
| dx1 | = 0 | P1 | = -6977.02 | Stress1 | = -1009.7 | Strain1 | = -4.80809E-04 |
| dy1 | = 0 | P2 | = -622.132 | Stress2 | = -90.0336 | Strain2 | = -4.28731E-05 |
| dx2 | = 0 | P3 | = 1394.21 | Stress3 | = 201.767 | Strain3 | = 9.60795E-05 |
| dy2 | = 0 | P4 | = 1518.8 | Stress4 | = 219.798 | Strain4 | = 1.04666E-04 |
| dx3 | = -0.0567054 | P5 | = 1648.21 | Stress5 | = 238.526 | Strain5 | = 1.13584E-04 |
| dy3 | = -0.0576971 | P6 | = -9033.08 | Stress6 | = -1307.25 | Strain6 | = -6.22499E-04 |
| dx4 | = -0.0203586 | P7 | = 2299.79 | Stress7 | = 332.821 | Strain7 | = 1.58486E-04 |
| dy4 | = 0.0125599 | P8 | = -3241.06 | Stress8 | = -469.04 | Strain8 | = -2.23352E-04 |
| dx5 | = -0.0459999 | P9 | = 3304.85 | Stress9 | = 478.271 | Strain9 | = 2.27748E-04 |
| dy5 | = -0.172734 | P10 | = -644.781 | Stress10 | = -93.3113 | Strain10 | = -4.44339E-05 |
| dx6 | = -0.0531093 | P11 | = -7865.19 | Stress11 | = -1138.23 | Strain11 | = -5.42016E-04 |
| dy6 | = 0.0302025 | P12 | = -1833.72 | Stress12 | = -265.372 | Strain12 | = -1.26367E-04 |
| dx7 | = -0.263159 | P13 | = 526.232 | Stress13 | = 76.1551 | Strain13 | = 3.62643E-05 |
| dy7 | = -0.237776 | P14 | = 3462.57 | Stress14 | = 501.095 | Strain14 | = 2.38617E-04 |
| dx8 | = -0.25127 | P15 | = 1078.31 | Stress15 | = 156.051 | Strain15 | = 7.43099E-05 |
| dy8 | = 0.0588365 | P16 | = -6424.98 | Stress16 | = -929.809 | Strain16 | = -4.42766E-04 |
| dx9 | = -0.521948 | P17 | = -1874.12 | Stress17 | = -271.219 | Strain17 | = -1.29152E-04 |
| dy9 | = -0.290908 | P18 | = 485.829 | Stress18 | = 70.3081 | Strain18 | = 3.34800E-05 |
| dx10 | = -0.53075 | P19 | = 2070.84 | Stress19 | = 299.687 | Strain19 | = 1.42708E-04 |
| dy10 | = 0.0759614 | P20 | = -798.311 | Stress20 | = -115.53 | Strain20 | = -5.50142E-05 |
| dx11 | = -0.693623 | P21 | = -1479.76 | Stress21 | = -214.148 | Strain21 | = -1.01975E-04 |
| dy11 | = -1.00876 | P22 | = 1805.92 | Stress22 | = 261.348 | Strain22 | = 1.24452E-04 |
| dx12 | = -0.681792 | P23 | = -4980.65 | Stress23 | = -720.789 | Strain23 | = -3.43233E-04 |
| dy12 | = 0.521926 | P24 | = -1272.47 | Stress24 | = -184.149 | Strain24 | = -8.76899E-05 |
| dx13 | = -0.848752 | P25 | = 694.156 | Stress25 | = 100.457 | Strain25 | = 4.78365E-05 |
| dy13 | = -0.332096 | P26 | = 1005.04 | Stress26 | = 145.447 | Strain26 | = 6.92605E-05 |
| dx14 | = -0.825256 | P27 | = -1805.92 | Stress27 | = -261.348 | Strain27 | = -1.24452E-04 |
| dy14 | = 0.0842727 | P28 | = 1479.76 | Stress28 | = 214.148 | Strain28 | = 1.01975E-04 |
| dx15 | = -1.16528 | P29 | = 2130.98 | Stress29 | = 308.391 | Strain29 | = 1.46853E-04 |
| dy15 | = -0.360055 | P30 | = -3380.97 | Stress30 | = -489.287 | Strain30 | = -2.32994E-04 |
| dx16 | = -1.18381 | P31 | = -1180.03 | Stress31 | = -170.771 | Strain31 | = -8.13195E-05 |
| dy16 | = 0.0875387 | P32 | = 393.273 | Stress32 | = 56.9136 | Strain32 | = 2.71017E-05 |
| dx17 | = -1.35803 | P33 | = 394.946 | Stress33 | = 57.1557 | Strain33 | = 2.72170E-05 |
| dy17 | = -1.54355 | P34 | = -1680.64 | Stress34 | = -243.219 | Strain34 | = -1.15818E-04 |
| dx18 | = -1.3524 | P35 | = -2043.66 | Stress35 | = -295.753 | Strain35 | = -1.40835E-04 |
| dy18 | = 0.676295 | P36 | = 2364.55 | Stress36 | = 342.192 | Strain36 | = 1.62949E-04 |
| dx19 | = -1.54015 | P37 | = -2265.76 | Stress37 | = -327.895 | Strain37 | = -1.56141E-04 |
| dy19 | = -0.378792 | P38 | = -797.433 | Stress38 | = -115.403 | Strain38 | = -5.49537E-05 |
| dx20 | = -1.51422 | P39 | = 382.542 | Stress39 | = 55.3606 | Strain39 | = 2.63622E-05 |
| dy20 | = 0.0868865 | P40 | = -78.869 | Stress40 | = -11.4138 | Strain40 | = -5.43512E-06 |
| dx21 | = -1.87792 | P41 | = -2364.55 | Stress41 | = -342.192 | Strain41 | = -1.62949E-04 |
| dy21 | = -0.389696 | P42 | = 2043.66 | Stress42 | = 295.753 | Strain42 | = 1.40835E-04 |
| dx22 | = -1.89437 | P43 | = 2351.23 | Stress43 | = 340.264 | Strain43 | = 1.62031E-04 |
| dy22 | = 0.0837891 | P44 | = -1318.53 | Stress44 | = -190.815 | Strain44 | = -9.08644E-05 |
| dx23 | = -2.06961 | P45 | = -423.286 | Stress45 | = -61.257 | Strain45 | = -2.91700E-05 |
| dy23 | = -1.18093 | P46 | = 363.364 | Stress46 | = 52.5852 | Strain46 | = 2.50406E-05 |
| dx24 | = -2.06786 | P47 | = -374.553 | Stress47 | = -54.2045 | Strain47 | = -2.58117E-05 |
| dy24 | = 0.612047 | P48 | = -1492.49 | Stress48 | = -215.99 | Strain48 | = -1.02852E-04 |



PRINT U NODAL SOLUTION PER NODE

***** POST1 NODAL DEGREE OF FREEDOM LISTING *****

LOAD STEP= 0 SUBSTEP= 1
TIME= 2.0000 LOAD CASE= 0

THE FOLLOWING DEGREE OF FREEDOM RESULTS ARE IN THE GLOBAL COORDINATE SYSTEM

| NODE | UX | UY | UZ | USUM |
|------|--------------|--------------|--------|-------------|
| 1 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 2 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| 3 | -0.56705E-01 | -0.57697E-01 | 0.0000 | 0.80898E-01 |
| 4 | -0.20359E-01 | 0.12560E-01 | 0.0000 | 0.23921E-01 |
| 5 | -0.46000E-01 | -0.17273 | 0.0000 | 0.17875 |
| 6 | -0.53109E-01 | 0.30202E-01 | 0.0000 | 0.61097E-01 |
| 7 | -0.26316 | -0.23778 | 0.0000 | 0.35467 |
| 8 | -0.25127 | 0.58836E-01 | 0.0000 | 0.25807 |
| 9 | -0.52195 | -0.29091 | 0.0000 | 0.59754 |
| 10 | -0.53075 | 0.75961E-01 | 0.0000 | 0.53616 |
| 11 | -0.69362 | -1.0088 | 0.0000 | 1.2242 |
| 12 | -0.68179 | 0.52193 | 0.0000 | 0.85863 |
| 13 | -0.84875 | -0.33210 | 0.0000 | 0.91141 |
| 14 | -0.82526 | 0.84273E-01 | 0.0000 | 0.82955 |
| 15 | -1.1653 | -0.36005 | 0.0000 | 1.2196 |
| 16 | -1.1838 | 0.87539E-01 | 0.0000 | 1.1870 |
| 17 | -1.3580 | -1.5435 | 0.0000 | 2.0559 |
| 18 | -1.3524 | 0.67630 | 0.0000 | 1.5121 |
| 19 | -1.5401 | -0.37879 | 0.0000 | 1.5860 |
| 20 | -1.5142 | 0.86887E-01 | 0.0000 | 1.5167 |
| 21 | -1.8779 | -0.38970 | 0.0000 | 1.9179 |
| 22 | -1.8944 | 0.83789E-01 | 0.0000 | 1.8962 |
| 23 | -2.0696 | -1.1809 | 0.0000 | 2.3828 |
| 24 | -2.0679 | 0.61205 | 0.0000 | 2.1565 |
| 25 | -2.2548 | -0.39418 | 0.0000 | 2.2890 |
| 26 | -2.2365 | 0.81970E-01 | 0.0000 | 2.2380 |

MAXIMUM ABSOLUTE VALUES

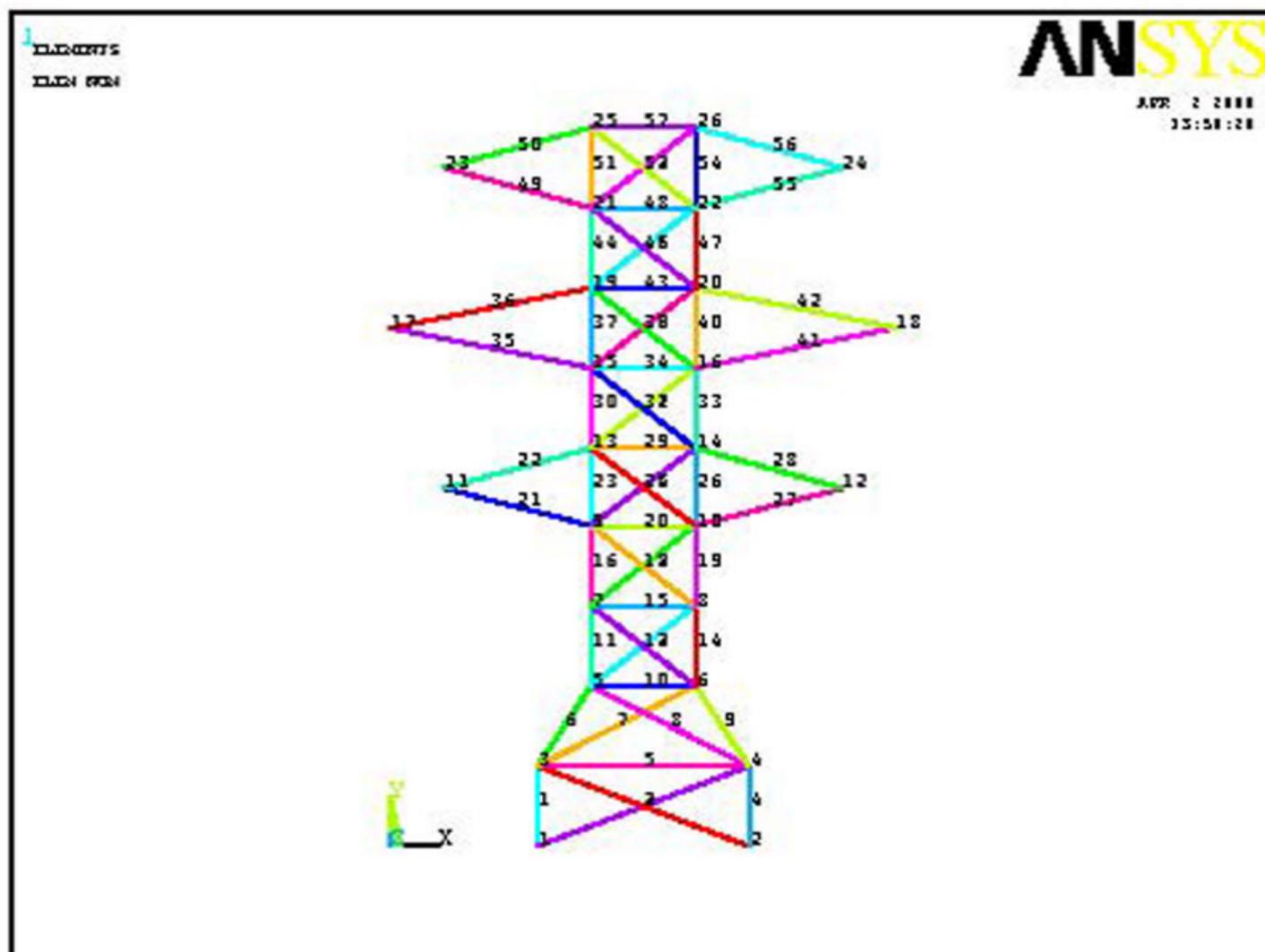
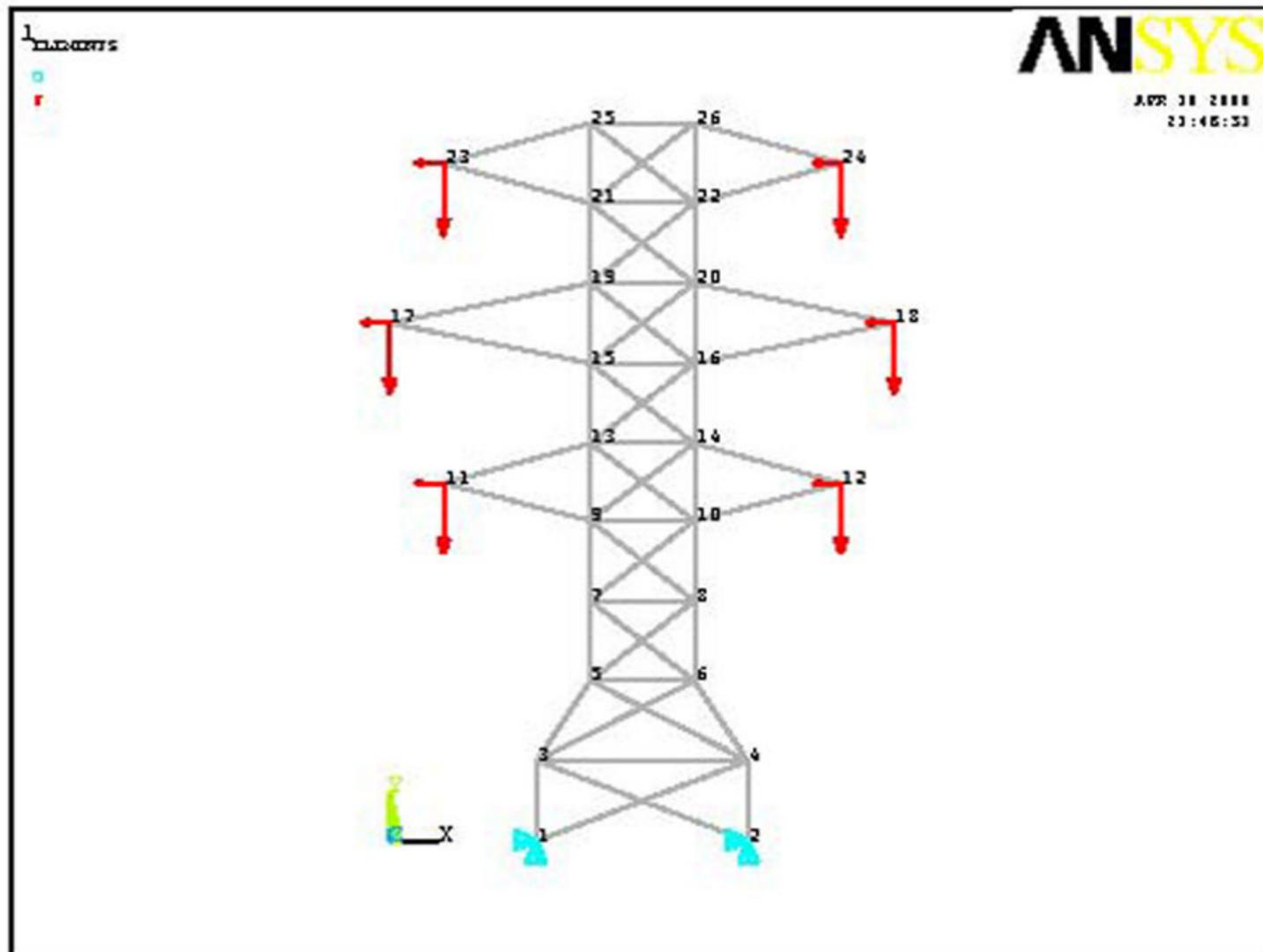
| NODE | 25 | 17 | 0 | 23 |
|-------|---------|---------|--------|--------|
| VALUE | -2.2548 | -1.5435 | 0.0000 | 2.3828 |

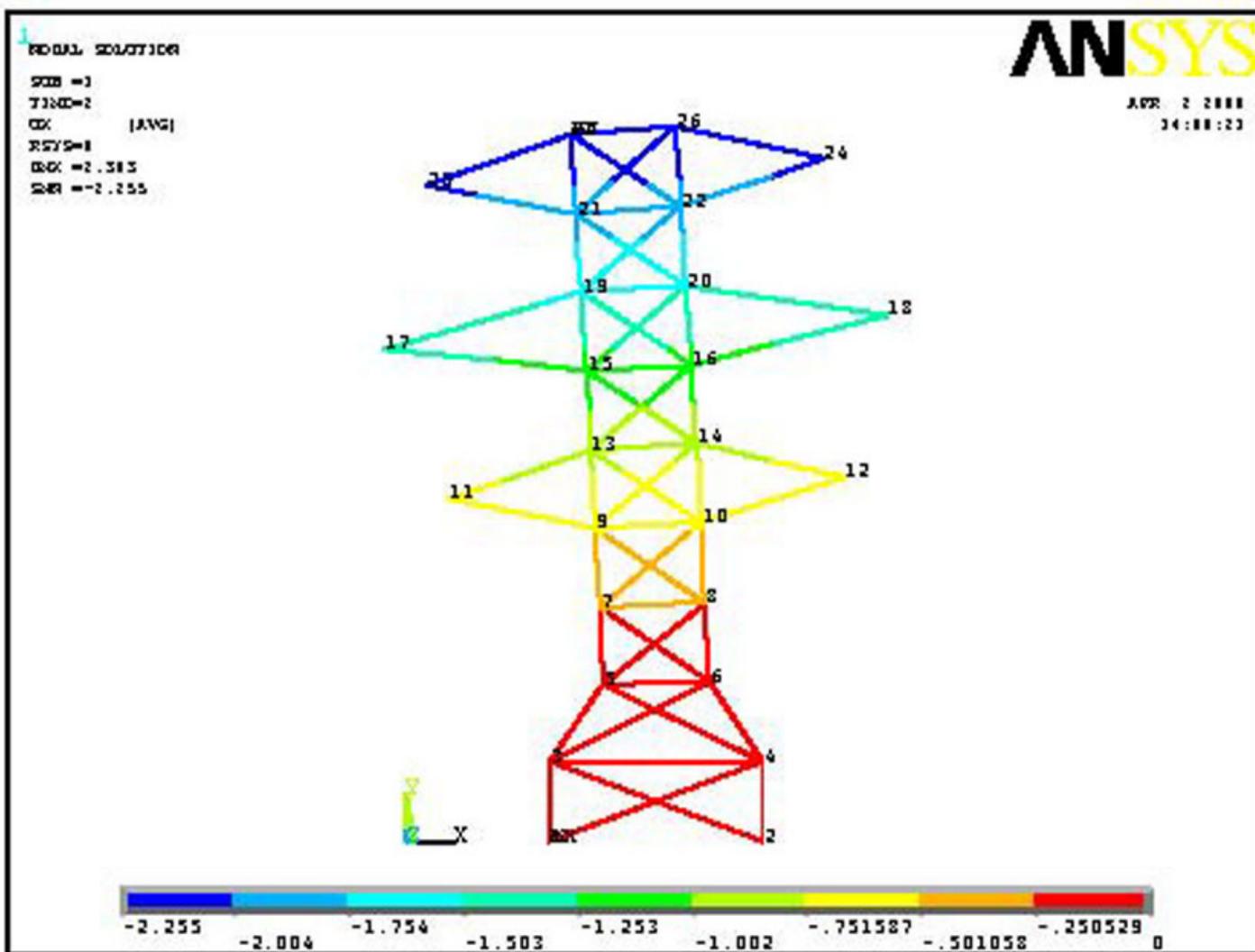
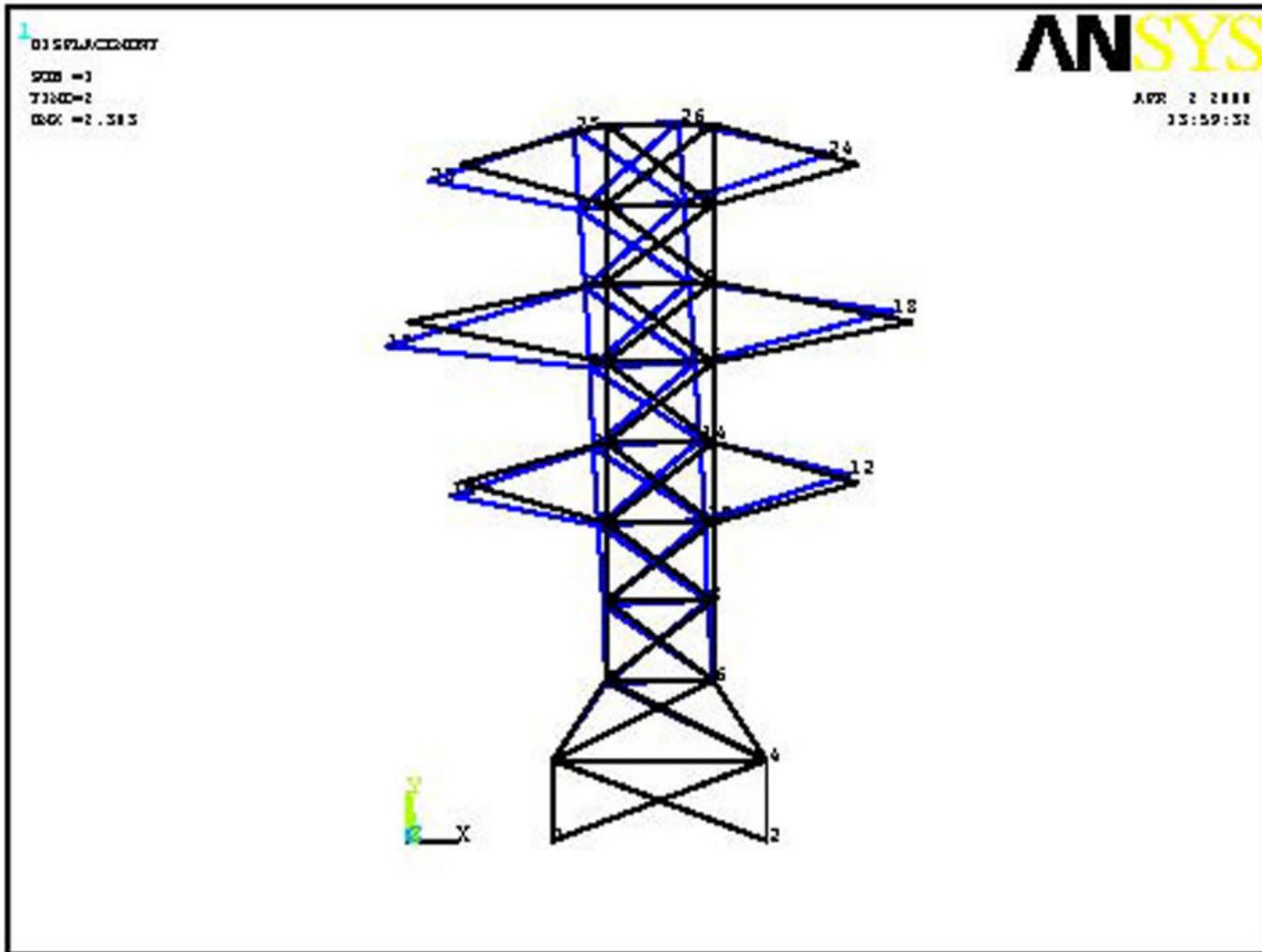


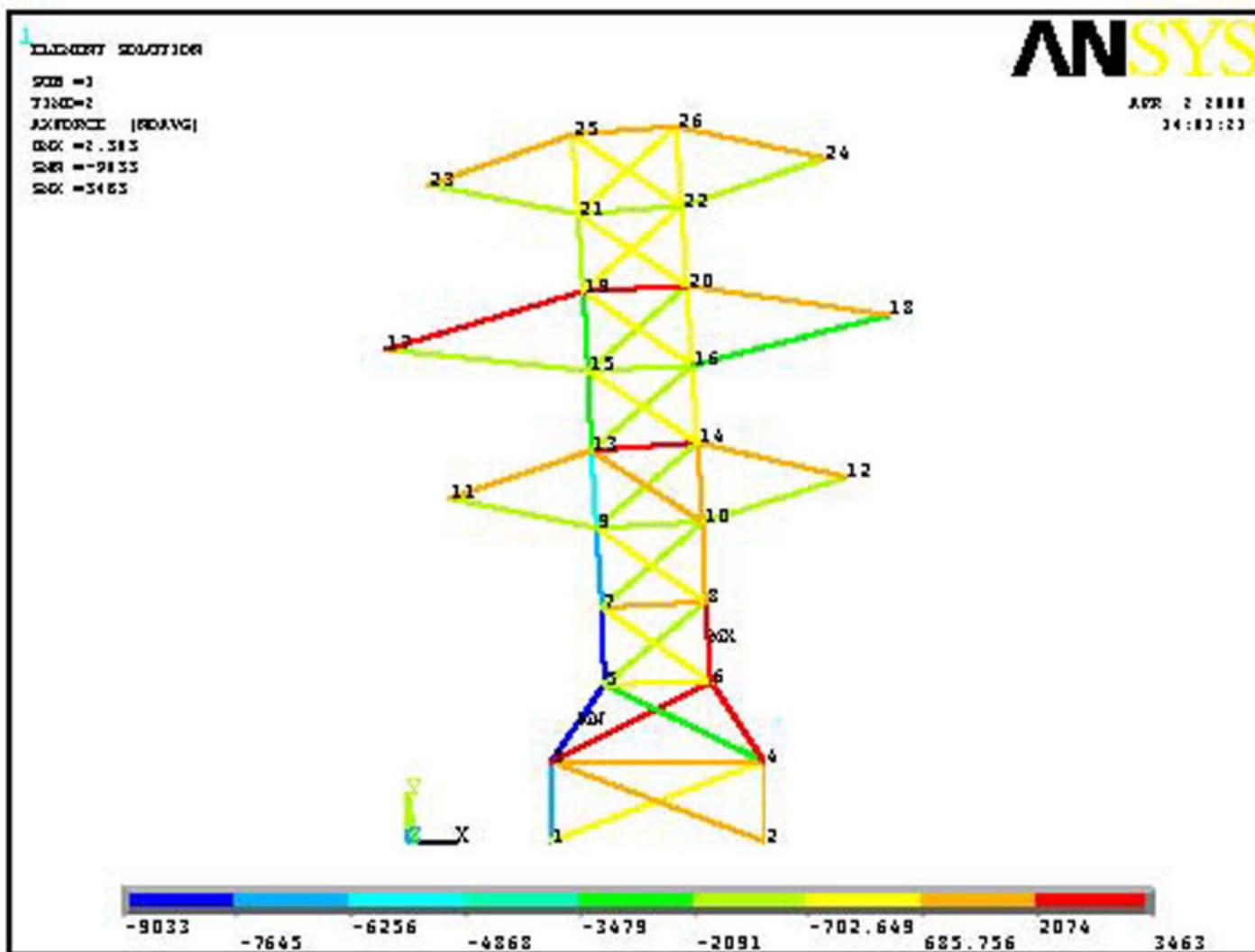
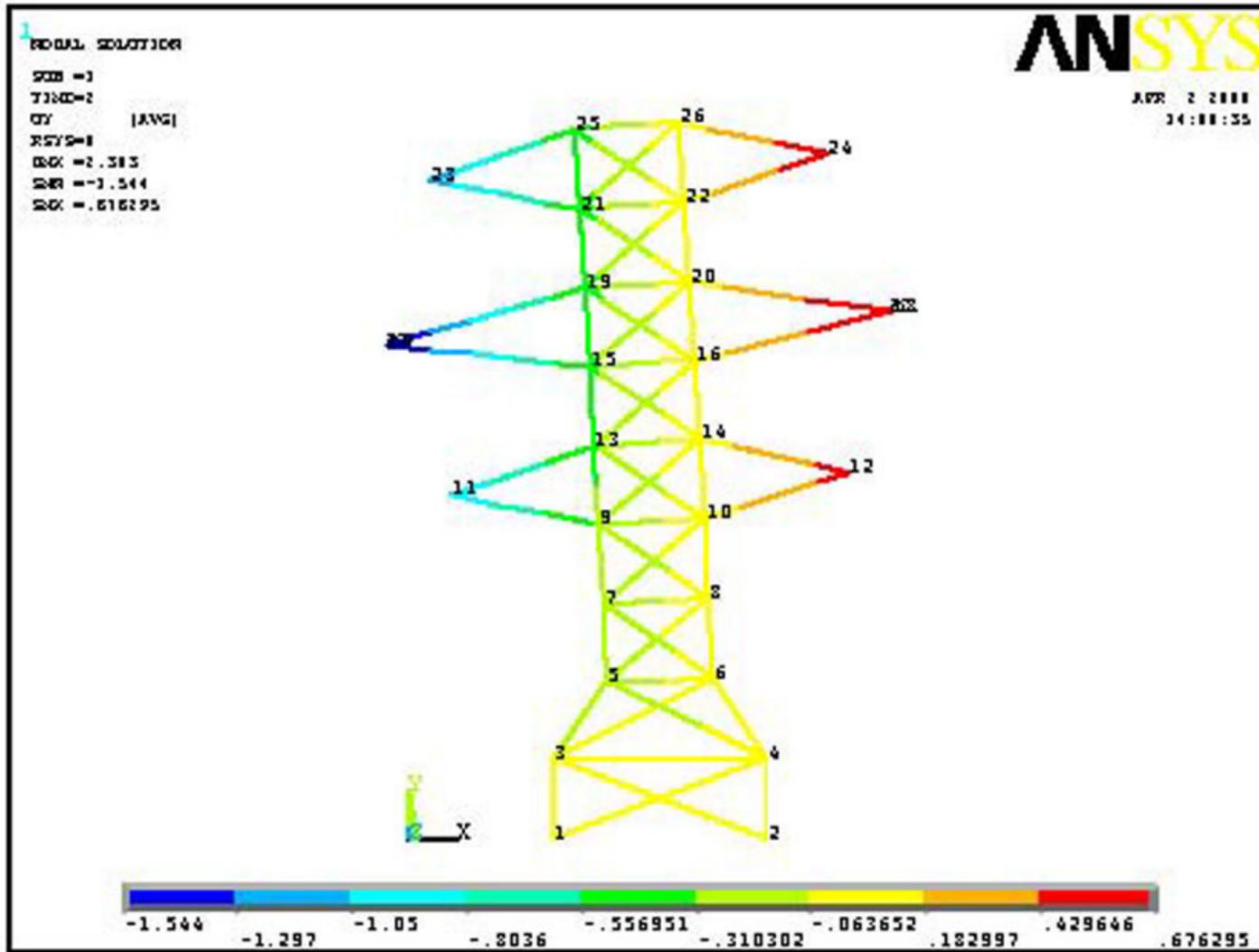
PRINT ELEMENT TABLE ITEMS PER ELEMENT

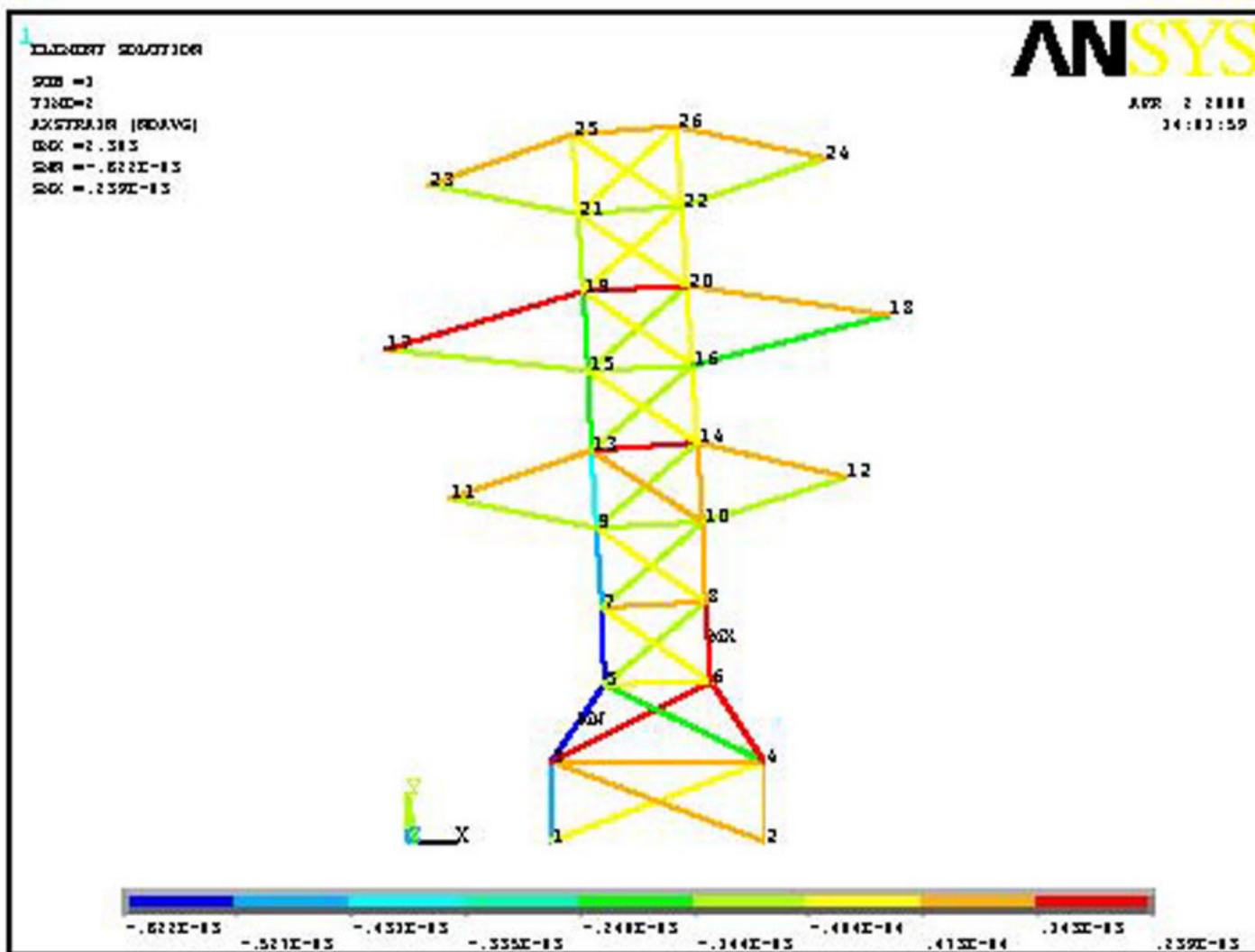
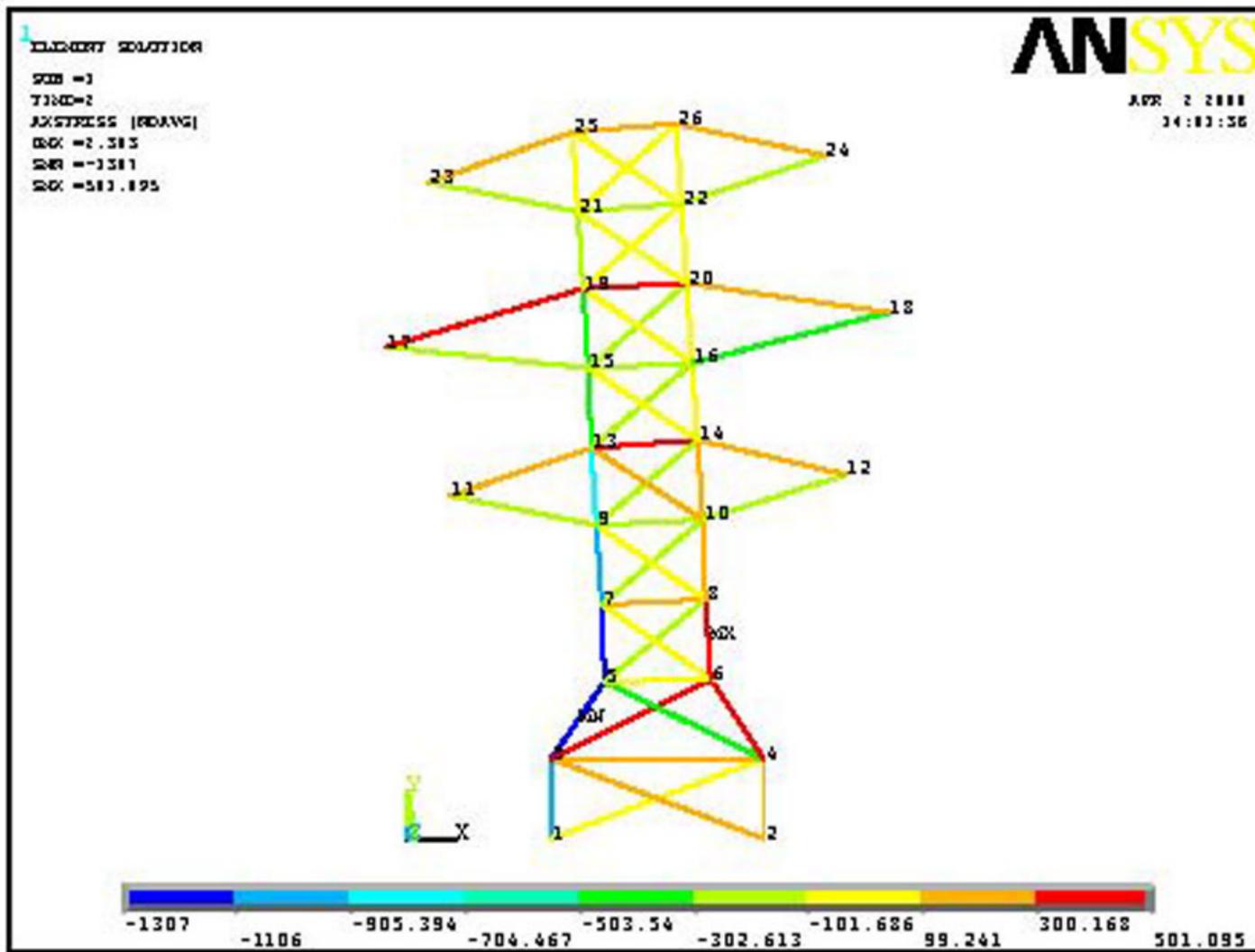
***** POST1 ELEMENT TABLE LISTING *****

| STAT ELEM | CURRENT AXFORCE | CURRENT AXSTRESS | CURRENT AXSTRAIN |
|--------------|--------------------|---------------------|---------------------|
| 1 | -6977.0 | -1009.7 | -0.48081E-03 |
| 2 | -622.13 | -90.034 | -0.42873E-04 |
| 3 | 1394.2 | 201.77 | 0.96080E-04 |
| 4 | 1518.8 | 219.80 | 0.10467E-03 |
| 5 | 1648.2 | 238.53 | 0.11358E-03 |
| 6 | -9033.1 | -1307.2 | -0.62250E-03 |
| 7 | 2299.8 | 332.82 | 0.15849E-03 |
| 8 | -3241.1 | -469.04 | -0.22335E-03 |
| 9 | 3304.9 | 478.27 | 0.22775E-03 |
| 10 | -644.78 | -93.311 | -0.44434E-04 |
| 11 | -7865.2 | -1138.2 | -0.54202E-03 |
| 12 | -1833.7 | -265.37 | -0.12637E-03 |
| 13 | 526.23 | 76.155 | 0.36264E-04 |
| 14 | 3462.6 | 501.09 | 0.23862E-03 |
| 15 | 1078.3 | 156.05 | 0.74310E-04 |
| 16 | -6425.0 | -929.81 | -0.44277E-03 |
| 17 | -1874.1 | -271.22 | -0.12915E-03 |
| 18 | 485.83 | 70.308 | 0.33480E-04 |
| 19 | 2070.8 | 299.69 | 0.14271E-03 |
| 20 | -798.31 | -115.53 | -0.55014E-04 |
| 21 | -1479.8 | -214.15 | -0.10198E-03 |
| 22 | 1805.9 | 261.35 | 0.12445E-03 |
| 23 | -4980.7 | -720.79 | -0.34323E-03 |
| 24 | -1272.5 | -184.15 | -0.87690E-04 |
| 25 | 694.16 | 100.46 | 0.47837E-04 |
| 26 | 1005.0 | 145.45 | 0.69261E-04 |
| 27 | -1805.9 | -261.35 | -0.12445E-03 |
| 28 | 1479.8 | 214.15 | 0.10198E-03 |
| 29 | 2131.0 | 308.39 | 0.14685E-03 |
| 30 | -3381.0 | -489.29 | -0.23299E-03 |
| 31 | -1180.0 | -170.77 | -0.81319E-04 |
| 32 | 393.27 | 56.914 | 0.27102E-04 |
| 33 | 394.95 | 57.156 | 0.27217E-04 |
| 34 | -1680.6 | -243.22 | -0.11582E-03 |
| 35 | -2043.7 | -295.75 | -0.14083E-03 |
| 36 | 2364.5 | 342.19 | 0.16295E-03 |
| 37 | -2265.8 | -327.90 | -0.15614E-03 |
| 38 | -797.43 | -115.40 | -0.54954E-04 |
| 39 | 382.54 | 55.361 | 0.26362E-04 |
| 40 | -78.869 | -11.414 | -0.54351E-05 |
| 41 | -2364.5 | -342.19 | -0.16295E-03 |
| 42 | 2043.7 | 295.75 | 0.14083E-03 |
| 43 | 2351.2 | 340.26 | 0.16203E-03 |
| 44 | -1318.5 | -190.82 | -0.90864E-04 |
| 45 | -423.29 | -61.257 | -0.29170E-04 |
| 46 | 363.36 | 52.585 | 0.25041E-04 |
| 47 | -374.55 | -54.205 | -0.25812E-04 |
| 48 | -1492.5 | -215.99 | -0.10285E-03 |
| 49 | -1479.8 | -214.15 | -0.10198E-03 |
| 50 | 1805.9 | 261.35 | 0.12445E-03 |
| 51 | -541.80 | -78.408 | -0.37337E-04 |
| 52 | -282.28 | -40.851 | -0.19453E-04 |
| 53 | 111.05 | 16.070 | 0.76526E-05 |
| 54 | -219.99 | -31.836 | -0.15160E-04 |
| 55 | -1805.9 | -261.35 | -0.12445E-03 |
| 56 | 1479.8 | 214.15 | 0.10198E-03 |
| 57 | 1653.4 | 239.28 | 0.11394E-03 |









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```
for i=1:Ns
    r=2*Support(i,1);
    if Support(i,2)==0
        NewCivil.com
    elseif Support(i,2)==1
        S(r-1,i)=0;
    end
end
```